



Chilmark School



HVAC Engineering Services

September 9, 2020

The Up Island Regional School Committee & the Town of Chilmark are seeking proposals from qualified engineers to provide the services necessary to accomplish the following:

Chilmark School HVAC System Project # 2020-10

The Town of Chilmark and the Up-Island Regional School District have approved a project to renovate and modernize the school's HVAC system. A previous engineering study identified two options for an electric heat pump approach to provide both heating and air conditioning for the school. The planning team has selected the Variable Refrigerant Flow (VRF) air-sourced heat pump option as most appropriate for the project.

We are soliciting bids for a contract to provide a construction-ready engineering design for the system as well as project management for the subsequent construction and installation of the equipment. Please see the attached Chilmark Elementary School Mechanical Assessment and Recommendations – Final Report (April 11, 2020) by TE2 Engineering, our phase 1 engineer.

I. The engineering design project will include:

- **Determination of the optimal code-compliant equipment set including the number and sizing of external and internal units as well as the recommended manufacturer(s);**
- **Development of engineering drawings and associated specifications for locating that equipment;**
- **Design and documentation of the appropriate control subsystem.**

As an additional option:

- **Project management for the subsequent installation and prove-out of the system, including assistance in the selection of local HVAC and electrical contractors, to ensure the compliance of the as-installed system with the engineering design;**

Note that the system to be designed should be capable of handling the full heating load for the building, but that the building owner wishes to utilize the existing oil-fired hot water system as a backup for a period of time.

II. The full HVAC design should encompass:

- VRF heat pumps with ducted air handlers for all classrooms/offices
- o Heat pumps to be located on stands on either the roof or ground with vibration isolation

- Air handlers to be supplemented by electric resistance heat
- Energy Recovery Ventilators (ERVs) for balanced ventilation (MERV 13 filters) and to serve as the exhaust system for the bathrooms
- All air handlers and ERVs to be located in attic spaces for sound mitigation
- Attic spaces to be insulated and air sealed as part of the conditioned envelope
- Hallways to be conditioned by ceiling cassettes or electric ceiling convectors recessed into the hallway ceilings (limited space)
- Reconfigured fire sprinkler system (attic spaces)
- Location for the installation of an appropriately sized back-up generator to power: heating, lights, kitchen/office, and limited outlets in building.
- Existing fin tube and oil burner to remain as supplemental heat for the foreseeable future and for potential severe weather conditions.

III. Specific deliverable will include:

- HVAC notes, narrative, and control logic
- HVAC zone plan
- HVAC ductwork layout (plain view)
- HVAC conceptual piping plan
- HVAC outdoor heat pump locations
- HVAC interior unit locations
- HVAC details
- HVAC equipment schedule

Designs recommended by the engineer will take into consideration all normal industry standards, with special focus on

- Building & Occupant Health
- Installation cost
- Operating cycles
- Operating costs
- Environmental Impact/Energy Efficiency

IV. Existing Systems

The building was constructed in 1998.

It was fitted with a two boiler system that provided domestic hot water to hand washing sinks in classroom, hot water to baseboard radiators, and hot water to heat exchangers in six (6) attic mounted

air handing units for forced hot air and to heat fresh air for the classrooms. The boilers ran separately and together to meet the design load for the building. This system was sufficient to the comfort needs of the occupants.

Several non-boiler system building issues came up that resulted in water damage from frozen pipes in the domestic water and fire suppression system.

The “flat roof” areas over the hallways received remedial thermal treatment with spray foam insulation after domestic water lines froze and leaked through the ceilings.

The Air Handlers in the uninsulated and ventilated attics were wrapped in insulation after (the rooves were designed as “air washed”) after the cold outside air caused one unit to go into “survival mode” during particularly cold weather, and a poorly installed section of the fire suppression system piping froze and burst flooding the classroom. Ceilings of classrooms also received additional insulation.

The Control system was modified at some point since construction when the PC controlled thermostats and outdated software/hardware were failing.

One of the two boilers has now failed. It was being replaced this summer, when the school decided to stop and consider the installation of non-fossil fuel heating. We are running successfully on one boiler at this time.

When the new ERVs were installed into the classrooms, the air handlers were disabled. We don’t know how they were disabled or if they were fully decommissioned in place.

With the disabling of the air handlers the classrooms stopped receiving heat from the forced hot air ceiling vents. This left some rooms colder as linear feet of baseboard covers was not all radiators. The installation of a donation “mini-split” in one classroom has made the room usable in the cold months again.

MGL Ch 7 sec. 44-58

Registration in the Commonwealth of Massachusetts required.

Minimum required Insurance of \$1,000,000.

Standard Designer application and Designer Evaluation forms required.

INFORMATIONAL MEETING: September 16, 2020 @ 1:00 PM on Zoom

<https://zoom.us/j/95414255150?pwd=cXRsaFBkNHNPMytUWnFKU1JoTnhzZz09> Meeting ID: 954 1425 5150 Passcode: 6452101

QUESTIONS: Are accepted in writing until **September 21, 202 @ 10:00 AM** via email or facsimile

PROPOSALS DUE: September 25, 2020 @ 2:00 PM

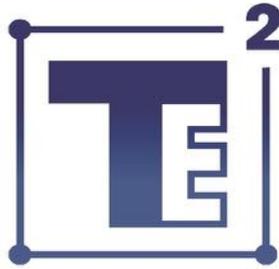
PROPOSALS should be sent to:

Town Administrator, PO Box 119, 401 Middle Road, Chilmark, MA 02535

QUESTIONS: Tim Carroll townadministrator@chilmarkma.gov

508-645-2101 voice 508-645-2110 facsimile

Request For Proposals (MGL Ch.7C) for Design Services for a comprehensive approach to convert the Chilmark Elementary School from Oil Heat to a Cold Climate Heat Pump HVAC system. Information: townadministrator@chilmarkma.gov. Deadline for proposals is September 25, 2020 at 2:00PM. Briefing Session: Sept 16, 2020 at 1:00PM sep11,1-t Vineyard Gazette.



TE2 ENGINEERING, LLC.

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www.te2engineering.com

April 11, 2020

Town of Chilmark
Attn: Tim Carroll
Chilmark Town Hall
401 Middle Road
PO Box 119
Chilmark, MA 02535-0199

Re: Chilmark Elementary School Mechanical Assessment and Recommendations - Final Report

Dear Mr. Carroll:

This letter and attached report serve to provide information pertaining to the overall energy use of the facility and the condition and operation of the existing mechanical systems as well as our recommendations to improve the overall energy and indoor environment of the school. Please read through this final report in full and let us know if you have any additional questions. Thank you.

Sincerely,

Ross Trethewey, PE, MSME
TE2 Engineering, LLC.

Introduction:

The Chilmark School, formerly the Menemsha School, is an elementary school in the town of Chilmark, Massachusetts on the island of Martha's Vineyard. The school educates students from Kindergarten through grade 5. The school student population is about 60 students who are supported by 10 teachers and staff.

The physical school building was constructed in 1998 and is a wood frame structure. The building is designed in the shape of a "U" with an inner courtyard and a total of 7 "pods". The pods resemble independent buildings all linked together by the common corridors. The satellite view of the school building to the right shows the layout of the school and the "pods". The pod in the center is the School Foyer and administrative offices while the other six are classrooms. There is a partial basement under the lower left pod where the boiler room is located.



Methodology:

The methodology for this study first involved a thorough and exhaustive review of the existing documentation, visits to the site and interviews with staff. The documentation included existing building floor plans as well as building elevations used for heat loss calculations. During the site visits, the mechanical equipment was assessed for condition to determine the remaining life expectancy.

Using the information gathered from the existing documentation and the site visits, a heating and cooling load calculation is done to determine the peak winter and summer energy demand. Finally, taking into consideration the condition of the existing equipment and piping as well as the goals of the project, a recommendation is made for the replacement system as well as feasibility of the alternative approaches.

Summary of Findings:

Overall Impressions

In general, the building has a history of underperforming HVAC systems. The system that exists today is far different than the original design intent. This original design intent was not a bad design but failed largely due to poor installation and workmanship. The subsequent modifications largely blamed the design for the flaws than the installation and addressed symptoms that presented themselves in different ways to different people. The end result is a bandaged system that doesn't perform on an energy basis or on comfort. The building as a whole would benefit from a comprehensive HVAC renovation to address the inadequacies outlined below in the individual components of the system.

Air Handling Units

In total, there are seven (7) existing air handling units located in the attic spaces. These air handling units are all made by McQuay International and consist of hot water heating coils. The main purpose of these units are to provide heating to the building and fresh air (ventilation air). The units appear to be manufactured approximately

in 1998, which means the units are beyond their useful life expectancy and should be removed during the next renovation. The design of this system seems to have been inadequate because in 2016, these units were disconnected from the hot water loop and electrical power was removed. In order to provide ventilation to the classrooms, energy recovery ventilators (ERV's) were installed in each classroom to compensate for the loss of the air handling units.

The air from the air handling units was distributed through ductwork between the ceiling and the roof. Ceiling diffusers throughout the spaces were intended to supply the air from the air handling unit evenly through the space. In the rooms with high, cathedral type ceilings, some of the supply diffusers were quite high in the space. Using this type of distribution for warm air can be ineffective due to the natural tendency for that warm air to stay at the peaks. Special "high throw" diffusers can be used to counteract that effect but none of the diffusers in these spaces are that type. In some cases, diffusers that were designed to "throw" the air in only 3 directions instead of 4 were installed incorrectly. Instead of "throwing" the air down, the diffusers were rotated to "throw" the air up; further enhancing the natural tendency for this warm air to stay at ceiling level.

This air distribution design is likely responsible or at least a major reason for the determination that the air handling unit design was inadequate; and ultimately disconnecting the system as a whole.

Heating Water Generation System including Boiler

The boiler room is located in the partial basement area. The hot water generation system consists of a single Buderus GB315 oil fired hot water boiler with a dedicated boiler pump, a pair of system distribution pumps arranged in lead/lag and associated piping, sensors and controls. The Buderus boiler replaced an existing cast iron section boiler that has been functionally disconnected but is still physically in the system. The oil is supplied from two tanks that are 275 gallons each. The system has a chemical treatment system.



Overall, the system could benefit from some upgrades and repairs. While the boiler is new and in good working order, there is evidence throughout the building of excess corrosion as is shown in the photo to the right. The source of the corrosion is unknown but it occurs in several locations throughout the system. This photo was taken at one of the air handling units in the attic.

Hot Water Terminal Units and Finned Tube Radiation

The main heating for the building is provided through baseboard finned tube radiation that is mounted along most of the perimeter of the building. In areas where finned tube radiation could not be installed, cabinet unit heaters were used. There is a hot water supply and return piping loop that travels through the corridor ceiling and taps off into each of the rooms. Each room is set up as an independently controlled zone with a separate thermostat. There are a total of 12 zones in this building.



Overall, the heating system is inadequate; largely because it was never intended as the sole source of heat. The original design intent was for the finned tube radiation and the air handling units to jointly provide the heating and ventilation for the spaces. Once the air handling units were disconnected, the sole source of heat remaining was an undersized finned tube radiation system. In addition to being undersized, the layout of the radiators does not allow for complete heating coverage

of all spaces; particularly the classrooms. Entire exterior exposures, where most of the heat is lost, are devoid of any kind of heat in each classroom.

Fortunately, the condition of the finned tube radiation is good. There are some missing end caps and other fittings randomly throughout the building but these can easily be replaced. Each zone also has a water balancing valve to ensure proper flow through each zone and a control valve that is wired to a dedicated thermostat. While each of the 12 zones has a dedicated thermostat, there are only 2 thermostats of the 12 that are the same model. The building is a random collection of thermostats; mostly made by Honeywell. There is no consistent standard within the building; which presents an additional challenge to the staff when trying to control or troubleshoot the spaces.

On the day of the site visit, there were several classrooms that felt too warm. There were doors left open to counteract the overheating. Interviews with the staff revealed that because of the random collection of thermostats, there wasn't anyone with sufficient knowledge of the thermostats to be able to control the rooms properly. It was also revealed during these interviews that during cold days, areas within the classrooms never get warm; which confirms the ineffective layout discussed earlier in this section.

Fresh Air Ventilation System

Originally, the ventilation for the building was provided through the air handling units with separate exhaust fans to maintain the air balance. As a result of various factors, the air handling units were disconnected and the building was left without a source for fresh air (aside from opening windows). The solution provided for the ventilation problem was to install a Renewaire energy recovery ventilator (ERV) in each classroom. These units use a set of fans to bring fresh air from outside and exhaust from inside simultaneously. An internal heat exchanger allows the energy from inside the building to be transferred to the air from the outside, which reduces the demand on the heating system. These units were installed in custom fabricated boxes and mounted either high on the wall in high ceiling areas or on the ceiling in flat ceiling areas. The supply air is distributed to the space with a fabric duct.



While this design meets the ventilation needs of the building, it presents new challenges that previously did not exist. First, the unit includes 2 fans that are now inside each classroom. When operating, these fans make noise.



The custom fabricated box that surrounds the ERV units likely makes that noise worse by reverberating the sound of the fans. The teachers commented that the noise can be very distracting to the learning process; and in some cases, the units were turned off as a result or their motion sensors were covered to prevent the ERV from operating. Secondly, while each unit has an energy recovery heat exchanger, there is no active control of the supply air temperature. The air that is supplied to the space on a cold day will still feel cold. Delivered supply air temperatures

from the ERV on a cold day could be in the 50 F range. This further burdens an already undersized finned tube radiation system. Since the cool supply air is delivered from ceiling level, the cool air tends to fall to the space (on top of the students) and creates a cold, drafty feeling.

The energy recovery units themselves are in very good condition because they've been protected in the boxes and they are relatively new. The problem with this installation is not the equipment but the application of the equipment. These types of systems can be very effective in providing fresh air to a building but should be used to pretreat ventilation air for an air handling unit rather than supplying air directly to the space or be provided with post heating capability to increase the delivered supply air temperature to the space at or above room temperature. Due to the age and condition of these units, it may be possible to reuse these units as part of a more appropriate solution. If they are to be reused, they should be located in the attic space where the sound can be properly dampened; and the supply air from these units should be further conditioned by an air handling unit or fan coil.

Air Conditioning Systems

The school currently does not contain any permanently installed air condition equipment in the majority of the spaces within the building. The only space with cooling is the Art Room where a single zone ductless split heat pump system has been installed. The installation of this unit was necessary for heating purposes and not for cooling (although it can provide cooling in the summer). The lack of cooling in the rest of the building is an area of focus for the recommendations later in the report.

HVAC System Upgrade Recommendations:

Considerations and Prerequisites

The most important consideration that TE2 Engineering was tasked with is to find a solution for the uneven heat distribution and the noise generated by the current ventilation system. In addition, the school has expressed a desire to move away from fossil fuel based energy sources. There are several options that can achieve these goals. These options are discussed below:

VRF System

A VRF (variable refrigerant flow) system uses a piping network to transport refrigerant throughout the building. Within each room, the refrigerant piping would connect to an indoor unit that can use the refrigerant to provide either heating or cooling at all times. At the other end of the refrigerant piping are air source heat pumps. These heat pumps capture heat from the outdoor air in heating mode and deliver the heat to the indoor units using the refrigeration cycle (driven with an electric compressor). In cooling mode, the cycle reverses and heat captured from inside the space is rejected to the outdoor air. There are several benefits to this system, the main being that this system is entirely electric and does not use any fossil fuel source. In addition, the indoor units are connected to a common refrigeration piping system which allows the sharing of energy. For example, on a cold but sunny day, a classroom with a southern exposure could benefit from cooling mode operation. The energy captured from this classroom could be used to provide heat in another classroom that has a northern exposure and isn't heated from the sun. Finally, the system allows the different spaces to be broken up into separate zones that can be controlled individually and heating or cooling can occur in different zones at the same time.



There are some negative aspects of this system however. The refrigerant that is used is toxic and this fluid is piped throughout the building. New codes and standards limit how much of this refrigerant can be present in a single system. While the code is designed to protect the health and safety of the building occupants, it can cause the cost of the system to increase significantly as the design could be forced to be broken up into smaller subsystems with lower refrigerant volumes. Finally, as this system is an air source system, the efficiency in heating mode suffers as the outdoor temperature falls. This can cause excessive electricity costs to accumulate during long periods of extreme cold weather.

Air-to-Water Heat Pump

An air-to-water heat pump (known as ATW heat pump) operates similarly to the VRF system described above but uses water as the means to transport energy from inside and outside. All of the toxic refrigerant stays outside of the building. This type of system still uses the outdoor air as a heat source in winter and rejects captured heat



from inside during summer. As compared to the VRF system, there are some advantages to an ATW heat pump system. First, as indicated above, all of the toxic refrigerant gas stays outside and away from the building occupants. Secondly, since the system uses water to transport energy from inside and outside, the existing piping distribution system would be reused (if determined to be sufficiently sized). Finally, like the VRF system, an ATW heat pump is entirely electric and also does not use any kind of fossil fuel.

An ATW heat pump and VRF system also share some of the same negative aspects. Like the VRF, the ATW heat pump efficiency is dependent on the outdoor air. When the outdoor temperature falls, so does the efficiency. One drawback that the ATW heat pump has that the VRF does not is the inability to provide heating and cooling at the same time in different spaces. While this can be achieved through a 4-pipe system, the costs to install separate heating and cooling piping becomes prohibitive. Also, since the ATW heat pump uses water and that water is piped outside where the heat pump is located, freezing becomes a concern. In northern climates, ATW heat pumps use a glycol antifreeze solution to protect against

freezing. Not only is this more expensive to maintain but lowers the overall efficiency of the system even more. Lastly, ATW heat pumps typically reach maximum supply water temperatures of ~120 F on cold days, so in a retrofit system that was originally designed for temperatures of 180 F+ (like from a boiler), this means the existing heating emitters will be undersized, and will require supplemental heat or additional heating emitters.

Hybrid System

An interesting approach to this building could be a hybrid approach; that is using several different types of systems that compliment each other rather than committing to a single solution. A hybrid system could utilize the existing infrastructure while supplementing with new systems to compensate for the shortcomings. One example of a hybrid system is to use an ATW heat pump to provide heating hot water to the existing baseboard system until the outdoor temperature becomes too cold; at which point the boilers turn on to supplement. While this still uses fossil fuels during the coldest periods of the winter, it would significantly decrease the amount of oil used, and provide redundancy.

Another example could combine an ATW heat pump with a VRF system. Again, the ATW heat pump could replace the boiler system and provide heated hot water for the existing finned tube system. The VRF system could then supplement each space to provide the final comfort and ventilation needed. This would provide an all electric system that benefits from the comfort of hydronic heating and supplements the comfort with the VRF system.

A final option for a hybrid system could be to combine the VRF system with supplemental electric heat for the coldest days of the year. A duct heater could be used on the outlet of the VRF air handling units to provide a “boost” on the coldest days of the year when the system efficiency is very low. While not as comfortable or efficient as a hydronic based system, this option would likely be the most cost effective solution.

Budget Estimates

The options described above lend themselves well to a menu type of cost estimate. Each item can be evaluated individually while also being combined with some of the other options. The costs shown below are the best engineering estimates available with the information gathered through the site visit, interviews with the staff, research into the existing equipment and our own energy calculations performed on the building (available in the appendix). It is recommended that these costs be verified by a qualified contractor prior to allocating funds to perform the work. Market conditions and availability of qualified labor personnel can have a significant effect on pricing as well as the nature of the location on an island. The New England region as a whole is currently experiencing a very tight labor market in the trades which results in higher than expected installation costs and longer than expected project timelines. These factors should also be considered when selecting the type of system to use because some technologies require specialist knowledge while others do not. The issue is further complicated by the recent Corona Virus pandemic. The costs outlined in the table below do not include all costs associated with the upgrade, for example, demolition of existing equipment, insulation of the roof, relocation of ERV’s/terminations, any ceiling, sprinkler system or patching/painting work that is required to be done as a part of this HVAC upgrade is not included. The cost for this additional work should be confirmed by a general contractor and respective subcontractors.

Description	Estimated Cost
VRF System	\$200,000
Air-to-Water Heat Pump for Heating Only	\$160,000
Supplemental Electric Heat for VRF System	\$20,000
Thermostat upgrades (applicable to all options)	\$10,000

The timeline for a project like this can vary greatly with the availability of qualified personnel. Due to the nature of this project being a school, the work must be completed during the summer. This work should not take more than 3 months to complete with an adequately staffed crew.

Conclusions & Recommendations

The first concern for this building is the ventilation system. The current classroom mounted ERV system is unacceptable for the nature of the building. Additionally, the building experiences uneven heating and a lack of cooling. With this in mind, there needs to be some architectural changes to the building to accommodate any of the options described above. The rooms with high cathedral ceilings do not have attic space to mount HVAC equipment. If the ceiling could be made flat in each pod this would allow an “attic space” for mechanical equipment to reside. Since this work needs to be performed to make space for new equipment, it is an ideal time to upgrade the insulation in the attic. Rather than adding additional batt insulation at ceiling level, a better option would be to use closed cell spray foam insulation on the roof joists. This would create a completely insulated and air sealed space within the attic that puts the mechanical equipment inside of the thermal envelope. This is currently not the case for the classrooms with a lowered ceiling, as those attics are vented, and the mechanical equipment experiences very cold and hot conditions. This would provide tremendous benefit to the space and the performance of the equipment. Additionally, acoustic isolation treatment can be added to the ceiling of each

classroom to reduce the mechanical noise transmission into the classroom. This, along with finishing the window upgrade project, would help reduce the heating load of the building and save money on the purchase of the new mechanical equipment.

During the ceiling work phase of the project, the fire sprinkler system will require modifications to adapt the sprinkler head locations to the new ceiling. Since the sprinkler piping will no longer be in an unheated attic space, it would be possible to convert the sprinkler system from a dry system to a wet system. The dry system was originally installed to prevent pipes from freezing and bursting. While this is an obvious advantage when there is a freeze condition, eliminating the freeze condition also eliminates the advantage of the dry system. A wet system would respond faster to a fire emergency and it would eliminate the need for the air compressor (which keeps the dry side of the system pressurized).

Once that work is complete, there are two options that make the most sense for this building. The first option makes more sense from a comfort perspective and that is the hybrid system consisting of the VRF system with the ATW heat pump. Hydronic based heating is a more comfortable type of heat because the operating temperature of the system prevents the space from feeling dry, as well as there are no air drafts/convective currents. A new ATW heat pump would be installed somewhere outside (or potential indoors and vented to the exterior); likely near the boiler room; and the piping tied into the existing hot water distribution system. The existing boiler and oil tanks would then be removed. From an operational perspective, the finned tube system would be controlled solely based on 2 factors; occupancy and outdoor temperature. The intention of this system would not be the sole heat source for the building but to address the “base load”, which is the heat loss mainly through the exterior walls. Since this load is dependent on the outdoor temperature, controlling the system as a single zone works quite well. As the outdoor temperature falls, the ATW heat pump will produce warmer water to compensate.



The current finned tube system should operate similar to this method and as experience has revealed, it does not provide enough heat and comfort to the space. To address this concern in addition to a means to incorporate ventilation into the classroom, a new VRF system would need to be installed in the newly constructed attic spaces with outdoor heat pumps located either on the roof or on the ground next to the building. The VRF system would consist of ducted air handling units that supply heated air to the spaces. This same system would also be able to provide air conditioning during the warmer months. To address the ventilation, the existing renewaire ERV units can be moved into the attic spaces and connected to the new air handling units. The control of the VRF system would be based on schedule and space temperature. When the space is unoccupied, the ERV would turn off and the VRF set points would be adjusted to consume less energy. Occupancy sensors could be used in the classrooms in lieu of strictly scheduling to better enhance the energy performance of the new system. By controlling the VRF system from a thermostat and the finned tube radiation based on outdoor temperature, neither system is competing with the other for control of the environment.

The second option is more cost effective but less comfortable. This system is the VRF with supplemental electric heat. With this option, all of the hot water finned tube, piping, boilers and cabinet unit heaters would either be removed or abandoned in place (preferably removed). The VRF system described in the first option would be installed in the new attic spaces. In locations where hot water cabinet /unit heaters were installed, new electric heaters could be used. In addition, new electric resistance duct heaters would be installed in the supply air ductwork for the VRF air handling units, to supplement the space during the coldest days of the year when the VRF

heat pumps lose efficiency. The control of this system would strictly be based on occupancy and space temperature. A thermostat in each space would signal the system to provide either heating or cooling. When in heating, if the supply temperature does not achieve the desired set point, the electric duct heaters would turn on to supplement. Again, as in the first option, the ERV would not operate when the space was not occupied.

Lastly, whichever upgrade is selected, the thermostats should all be standardized. Simple to use thermostats are available, and by standardizing throughout the building, all teachers would have proper understanding and control of the HVAC system. In addition, many thermostats are WiFi enabled, which would allow the facilities manager or administrator to see all of the temperatures of the building from a single web enabled dashboard. This would allow temperature adjustments to be made remotely, including schedule adjustments, as well as provide alerts based on low temperature or high temperature limits being exceeded (or other similar conditions). This is far more cost effective than ever before.

In conclusion, both HVAC upgrade options meet the primary goals of addressing the uneven heating and the noise generated from the ERV units with an all electric system. While budget is always a concern, comfort of the occupants within the space should be an important consideration within the decision making process, as well as future operating costs/greenhouse gas emissions. If the proposed systems are evaluated at the present time, efficiencies of VRF heat pumps are approximately 3X that of an oil fired hydronic heating system (Seasonal Heat Pump COP= 2.5-3.0, Boiler COP= 0.85). However the price per gallon of oil, at \$2.80/gallon is equivalent to ~\$0.07/kWh, which is about one third of the electricity cost on the island (\$0.25/kWh). So this puts the operational costs of electrically driven VRF heat pumps “on par” with oil fired hydronic heating systems. Part of this is because the cost of electricity on the island is higher than the state average and much higher than the national average. So it is possible that the VRF and electric resistance heat system would have equal (or potentially higher) operating cost than that of the current oil fired system. This will largely depend on the price of oil/electricity and the extent of the energy currently being wasted through open windows and other inefficiencies/measures to control the indoor comfort. Additionally, the building currently does not have an air conditioning system (except for 1 classroom), so the use of air conditioning during the warmer months will certainly add to the operating costs of the building.

TE2 does not have any insight in terms of predicting future energy costs. If the goal is to ultimately reduce the electrical operating cost of the proposed HVAC solution, gain energy independence, hedge against energy inflation, lower Greenhouse Gas (GHG) emissions and care for the environment than the installation of on-site electrical generation with either solar panels or wind energy should be considered in conjunction with an all electric HVAC system. If the main goal is to reduce operating costs with minimal capital expenditure, in addition to hedging against variable future energy costs, then a dual fuel “hybrid” approach should be considered. This would leave the boiler and oil tanks in place, in the event that oil prices drop in the future, and could run in conjunction with the VRF heat pump system (referred to as covalent and bivalent control strategies).

Ultimately, any of the proposed options would offer a marked improvement of the current HVAC situation at the school, and all should be considered.

Appendix:

- Heating and Cooling Load Calculations
- WiFi Thermostat (Honeywell Vision Pro 8000 WiFi)- reference document for classrooms
- VRF cold climate heat pump (Mitsubishi PVA36-PUZ36 “Hyperheat”)- reference document for classrooms
- Air to Water Heat Pump (Aermec NRK 550)- reference document for example AWHP



Right-Suite® Universal 2019 Load Summary
Entire House

Job: Chilmark Elementary Sc...
 Date: March 3, 2020
 By: SRM

372 University Avenue, Westwood, MA 02090

Project Information

For: Chilmark Elementary School
 8 State Rd., Chilmark, MA 02535

Zone: Entire House

COOLING LOAD

1. DESIGN CONDITIONS	at Jul 1800 LDT	Peak load at Jul 1800 LDT		
Inside:	75 °F	Outside:	87 °F	TD: 12 °F
RH:	63 %	MoistDiff:	58.6 gr/lb	Mult: 1.0
				Ins.wb 63 °F
2. SOLAR RADIATION THROUGH GLASS			Sensible	Latent
			75258	-
3. TRANSMISSION GAINS			Sensible	Latent
			52311	-
Walls:	15943		-	-
Glass:	8470		-	-
Doors:	2527		-	-
Partitions:	0		-	-
Floors:	0		-	-
Ceilings:	25370		-	-
4. INTERNAL HEAT GAIN			Sensible	Latent
Occupants:	24242		58678	17970
Lights:	28715		17970	-
Motors:	0		-	-
Appliances:	5721		-	-
5. INFILTRATION:	Outside air cfm:		1256	16924
6. SUBTOTAL:	Space load		Sensible	Latent
Envelope	203171		203171	67979
Less external	0		-	-
Redistribution	0		0	-
7. SUPPLY DUCT			0	-
8. SUBTOTAL:	Space load + supply duct		203171	-
Actual cfm:	9433	at supply TD:	20	-
9. VENTILATION:	Make-up air cfm:		4064	19159
10. RETURN AIR LOAD:	Lighting + plenum (net)		0	80877
11. RETURN DUCT			0	-
12. TOTAL LOADS ON EQUIPMENT			222330	148856

HEATING LOAD

13. DESIGN CONDITIONS		Mult:	1.0
Inside:	70 °F	TD:	61 °F
Outside:	10 °F		
14. TRANSMISSION LOSSES			154199
Walls:	29844		-
Glass:	44857		-
Doors:	3356		-
Partitions:	0		-
Floors:	52575		-
Ceilings:	23566		-
15. INFILTRATION:	Outside air cfm:		2098
16. SUBTOTAL:	Space load		139464
Envelope	293663		293663
Less external	0		-
Less transfer	0		-
Redistribution	0		-
17. SUPPLY DUCT:			0
18. VENTILATION:	Make-up air cfm:		4064
19. HUMIDIFICATION			94546
Piping			0
20. RETURN DUCT			0
21. TOTAL HEATING LOAD ON EQUIPMENT			388209



Building Analysis

Entire House

Job: Chilmark Elementary Sc...
 Date: March 3, 2020
 By: SRM

372 University Avenue, Westwood, MA 02090

Project Information

For: Chilmark Elementary School
 8 State Rd., Chilmark, MA 02535

Design Conditions

Location:

Marthas Vineyard, MA, US
 Elevation: 33 ft
 Latitude: 41°N

Outdoor:

Dry bulb (°F)
 Daily range (°F)
 Wet bulb (°F)
 Wind speed (mph)

Heating

10
 -
 -
 15.0

Cooling

87
 16 (M)
 77
 7.5

Indoor:

Indoor temperature (°F)
 Design TD (°F)
 Relative humidity (%)
 Moisture difference (gr/lb)

Heating

70
 61
 37
 25.5

Cooling

75
 12
 50
 58.6

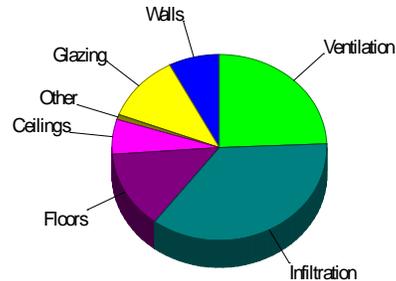
Infiltration:

Method
 Construction quality

Simplified
 Average

Heating

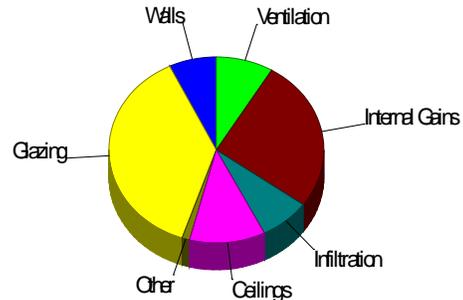
Component	Btuh/ft²	Btuh	% of load
Walls	3.8	29844	7.7
Glazing	19.4	44857	11.6
Doors	16.0	3356	0.9
Ceilings	1.9	23566	6.1
Floors	4.2	52575	13.5
Infiltration	55.2	139464	35.9
Ducts		0	0
Piping		0	0
Humidification		0	0
Ventilation		94546	24.4
Adjustments		0	0
Total		388209	100.0



Cooling

Jul 1800 LDT

Component	Btuh/ft²	Btuh	% of load
Walls	2.1	15943	7.2
Glazing	36.1	83728	37.7
Doors	12.0	2527	1.1
Ceilings	2.0	25370	11.4
Floors	0	0	0
Infiltration	6.7	16924	7.6
Ducts		0	0
Ventilation		19159	8.6
Internal gains		58678	26.4
Blower		0	0
Adjustments		0	0
Total		222330	100.0



Latent Cooling Load = 148856 Btuh
 Overall U-value = 0.077 Btuh/ft²-°F

Data entries checked.

Bold/italic values have been manually overridden



Right-Suite® Universal 2019 Short Form

Entire House

Job: Chilmark Elementary Sc...
 Date: March 3, 2020
 By: SRM

372 University Avenue, Westwood, MA 02090

Project Information

For: Chilmark Elementary School
 8 State Rd., Chilmark, MA 02535

		Htg	Clg			Htg	Clg
Outside db	(°F)	10	87	Inside db	(°F)	70	75
Outside RH	(%)	-	63	Inside RH	(%)	-	50
Outside wb	(°F)	-	77	Inside wb	(°F)	-	63
Daily range	(°F)	-	16	Design TD	(°F)	61	12
Moisture diff.	(gr/lb)	-	59				

Heating Equipment

Make			
Model			
Type	Gas furnace		
Efficiency	80 AFUE		
Heating Input	0	MBtuh	
Heating Output	0	MBtuh	
Humidifier	9.2	gpd	
Leaving Air Temp	70.0	°F	
Actual Heating Fan	9433	cfm	

Cooling Equipment

Make			
Model			
Type	Split AC		
COP / EER / SEER	0		
Sensible Cooling	0	MBtuh	
Latent Cooling	0	MBtuh	
Total Cooling	0	MBtuh	
Leaving Air Temp	55.0	°F	
Actual Cooling Fan	9433	cfm	

Equipment Location	Entire House
System Type	PEAKCV
Fan Motor Heat Type	PACKAGE
Fan & Motor Combined Efficiency	0 %
Static Pressure Across Fan	0 in H2O

NAME	Area ft²	Heat Loss	Sensible Gain	Latent Gain	Htg cfm	Clg cfm	Time
001 Storage	754	0	0	0	0	0	Jul 1800 LDT
002 Mechanical	645	0	0	0	0	0	Jul 1800 LDT
109 Airlock/Bell	260	18429	6938	3883	571	353	Jul 1800 LDT
110 Lobby	1521	52767	28528	14685	1570	1262	Jul 1800 LDT
111 Reception	217	3927	1859	1325	108	80	Jul 1800 LDT
112 Girls	134	1483	1026	924	37	44	Jul 1800 LDT
113 Boys	130	1442	1005	906	36	43	Jul 1800 LDT
114 Janitor	27	299	415	406	7	18	Jul 1800 LDT
115 Side Entrance	102	11554	5259	3117	363	246	Jul 1800 LDT
116 Stg.	78	863	706	653	21	30	Jul 1800 LDT
117 Principal	182	3545	1662	1158	99	72	Jul 1800 LDT
118 Conference	197	2185	1388	1231	54	58	Jul 1800 LDT
119 Nurse	122	1349	957	865	33	41	Jul 1800 LDT
120 Staff	76	836	692	641	21	30	Jul 1800 LDT
121 K 1	1332	40121	20696	17849	821	811	Jul 1800 LDT
122 K 1 Restroom	68	747	646	602	18	28	Jul 1800 LDT
123 Art/Music	786	25290	13865	11301	536	576	Jul 1800 LDT
125 Stg	123	2347	1200	869	65	52	Jul 1800 LDT
126 Tech	798	18819	14391	9850	384	592	Jul 1800 LDT

128 Hall W	689	29247	26242	5960	883	1191	Jul 1800 LDT
129 Hall E	670	28977	14633	5868	876	758	Jul 1800 LDT
130 Class-Room	1194	32219	15146	16191	616	562	Jul 1800 LDT
131 Class-Room	1178	33411	18847	16005	659	727	Jul 1800 LDT
132 Special Ed.	204	3600	2308	1263	99	104	Jul 1800 LDT
133 Class Room	1175	31134	20071	15966	587	795	Jul 1800 LDT
134 Class-Room	1183	39475	21681	16061	853	867	Jul 1800 LDT
135 Meeting	207	4139	2170	1278	116	94	Jul 1800 LDT
Entire House	14050	388209	222330	148856	9433	9433	Jul 1800 LDT



Component Constructions

Entire House

Job: Chilmark Elementary Sc...
 Date: March 3, 2020
 By: SRM

372 University Avenue, Westwood, MA 02090

Project Information

For: Chilmark Elementary School
 8 State Rd., Chilmark, MA 02535

Design Conditions

	Htg	Clg		Htg	Clg
Outside db (°F)	10	87	Inside db (°F)	70	75
Outside RH (%)	80	63	Inside RH (%)	37	50
Outside wb (°F)	20	77	Inside wb (°F)	55	63
Daily range (°F)	-	16	Design TD (°F)	61	12
Moisture diff. (gr/lb)	25.5	58.6			

Construction descriptions

Walls

Bg wall, heavy dry or light damp soil, concrete wall, 10" thk, 1/2" gypsum board int fnsh

	Or	Area ft²	U-value (Btuh/ft²-°F)	UA (Btuh/°F)	Loss (Btuh)	Gain (Btuh)
Bg wall, heavy dry or light damp soil, concrete wall, 10" thk, 1/2" gypsum board int fnsh	ne	510	0.09	46.7	0	0
	se	318	0.09	29.0	0	0
	sw	510	0.09	46.7	0	0
	nw	276	0.09	25.2	0	0
	all	1613	0.09	148	0	0
Frm wall, wd ext, 3/8" wood shth, r-11 cav ins, 1/2" gypsum board int fnsh, 2"x6" wood frm, 16" o.c. stud	ne	1659	0.08	133	8038	3512
	se	1579	0.08	126	7648	4465
	sw	1642	0.08	131	7955	5301
	nw	1281	0.08	103	6204	2665
	all	6160	0.08	493	29844	15943

Partitions

(none)

Windows

2 glazing, clr low e, U-0.32, SHGC-0.4, wood frame, French door; 6.67 ft head ht

		htg	clg	htg	clg		
2 glazing, clr low e, U-0.32, SHGC-0.4, wood frame, French door; 6.67 ft head ht	ne	54	0.32 / 0.32	17.3 / 17.3	17.3	1045	1022
	se	54	0.32 / 0.32	17.3 / 17.3	17.3	1045	1317
	sw	108	0.32 / 0.32	34.6 / 34.6	34.6	2091	5459
	nw	162	0.32 / 0.32	51.8 / 51.8	51.8	3136	7459
	all	378	0.32 / 0.32	121 / 121	121	7318	15257
2 glazing, clr low e, U-0.32, SHGC-0.4, wood frame, operable; 7.5 ft head ht	ne	620	0.32 / 0.32	198 / 198	198	12003	11996
	se	315	0.32 / 0.32	101 / 101	101	6098	7685
	sw	541	0.32 / 0.32	173 / 173	173	10474	27451
	nw	463	0.32 / 0.32	148 / 148	148	8964	21339
	all	1939	0.32 / 0.32	620 / 620	620	37539	68471

Doors

Door, wd sc type

Door, wd sc type	ne	42	0.33	13.9	839	327	
	sw	84	0.33	27.7	1678	1536	
	nw	42	0.33	13.9	0	0	
	nw	42	0.33	13.9	839	664	
	all	210	0.33	69.3	3356	2527	

Ceilings					
Rf/clg ceiling, wood shingles roof mat, frm cons, 1/2" gypsum board int fnsh, 6" thkns, r-44 ceil ins	13k	0.03	390	23566	25370
Floors					
Bg floor, heavy dry or light damp soil, 10' depth	1399	0.02	23.9	0	0
Bg floor, heavy dry or light damp soil, on grade depth	736	1.18	869	52575	0



Loads for Multiple Orientations

Entire House

Job: Chilmark Elementary Sc...
 Date: March 3, 2020
 By: SRM

372 University Avenue, Westwood, MA 02090

Project Information

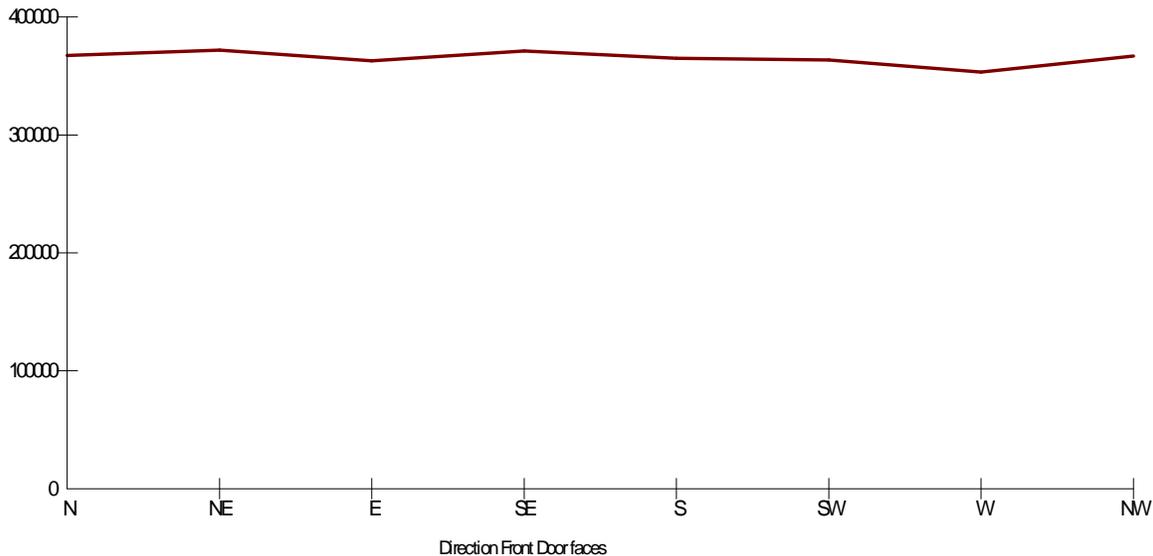
For: Chilmark Elementary School
 8 State Rd., Chilmark, MA 02535

Design Conditions

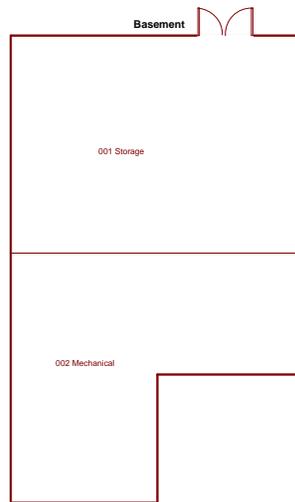
Location:				Indoor:	Heating	Cooling
Marthas Vineyard, MA, US				Indoor temperature (°F)	70	75
Elevation:	33 ft			Design TD (°F)	61	12
Latitude:	41°N			Relative humidity (%)	37	50
Outdoor:		Heating	Cooling	Moisture difference (gr/lb)	25.5	58.6
Dry bulb (°F)		10	87	Infiltration:		
Daily range (°F)		-	16 (M)			
Wet bulb (°F)		-	77			
Wind speed (mph)		15.0	7.5			

Front Door	North	Northeast	East	Southeast	South	Southwest	West	Northwest
Sensible Load (Btuh)	218432	223144	214056	222330	216060	214690	204501	218127
Latent Load (Btuh)	148856	148856	148856	148856	148856	148856	148856	148856
Total Load (Btuh)	367288	372001	362912	371187	364917	363546	353358	366984
Heating AVF (cfm)	9696	9660	9055	9433	9497	9388	8906	9510
Cooling AVF (cfm)	9696	9660	9055	9433	9497	9388	8906	9510

Building Orientation Cooling Load



Current Orientation: Front Door faces Southeast
 Highest Cooling Load: Front Door faces Northeast



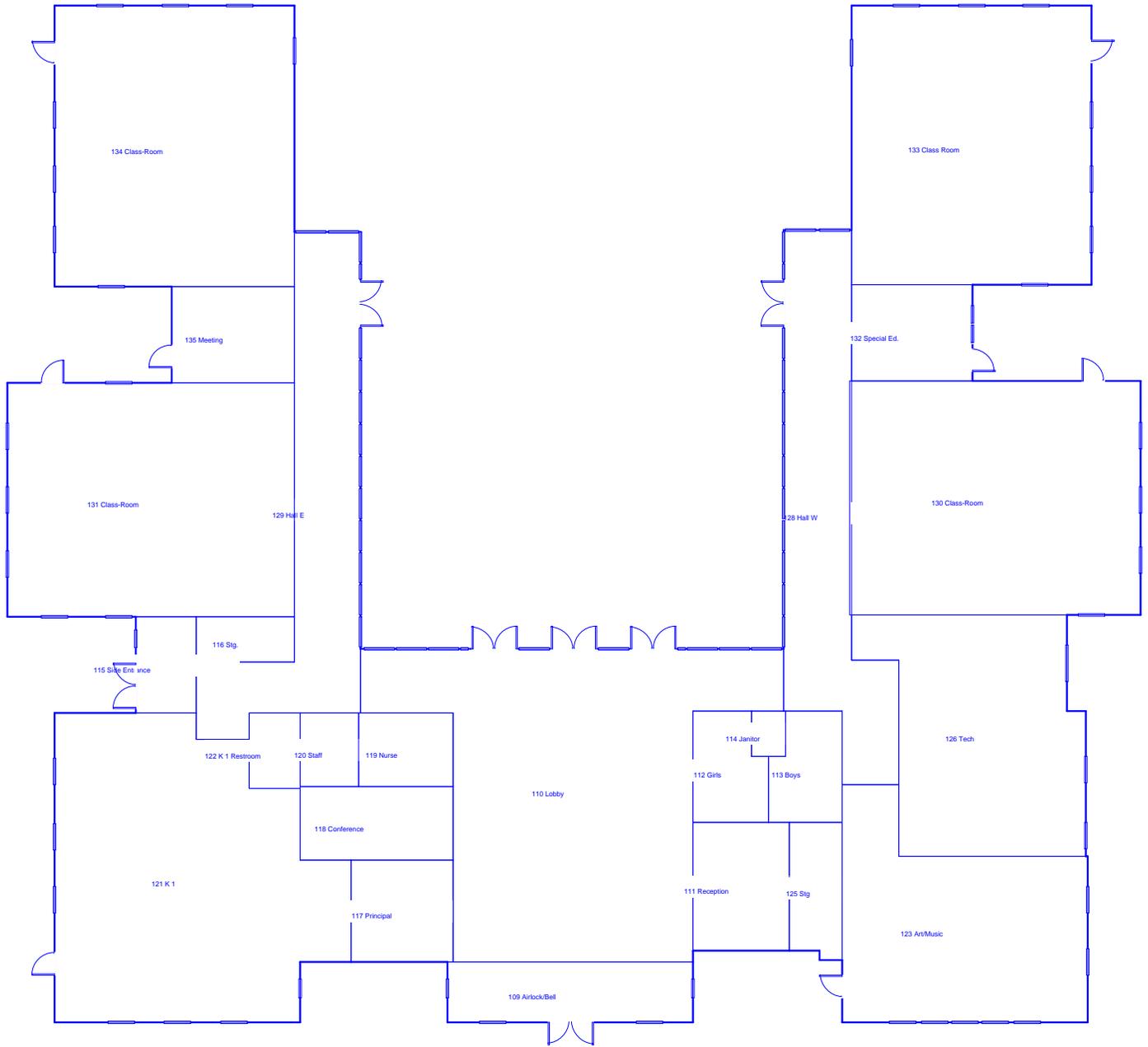
Job #: Chilmark Elementary School
Performed by SRM for:
Chilmark Elementary School
8 State Rd.
Chilmark, MA 02535

372 University Avenue
Westwood, MA 02090

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First Floor



Job #: Chilmark Elementary School
Performed by SRM for:
Chilmark Elementary School
8 State Rd.
Chilmark, MA 02535

372 University Avenue
Westwood, MA 02090

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Wi-Fi VisionPRO® 8000

SUBMITTAL SHEET

APPLICATION

Wi-Fi VisionPRO allows remote access through a Smartphone, Tablet or Computer. It controls Up to 3H/2C Heat Pump systems or up to 2H/2C Conventional systems. Thermostat is selectable for Residential or Light Commercial applications. The thermostat have a Universal Relay to control humidification, humidification or ventilation.

- The thermostat is equipped with a touchscreen display with a 2 line message center.
- Provides Remote Access through Smartphone, Tablet or Computer when connected to Wi-Fi and registered to mytotalconnectcomfort.com
- Provides lockout temperatures for auxiliary heat and/or compressor lockout in Heat Pump system using the wired outdoor sensor accessory or using the outdoor information from the cloud if no wired sensor is used, but the thermostat is connected to Wi-Fi and registered.

SPECIFICATIONS

Terminal Designations:

TH8321WF Thermostat: R, RC, C, W-O/B, W2-AUX/E, Y, Y2, G, A-L/A, K, U1 U1, S1 S1

Electrical Ratings (for VisionPRO and Equipment Interface Module):

Terminal	Voltage (50/60 Hz)	Max. Current Rating
W - O/B	18 to 30 VAC	1.00A
Y (cooling)	18 to 30 VAC	1.00A
G (fan)	18 to 30 VAC	0.50A
W2 - Aux/E	18 to 30 VAC	0.60A
Y2 (cooling)	18 to 30 VAC	0.60A
A-L/A (Output)	18 to 30 VAC	1.00A
U1, U1	30 VAC max.	0.50A

Power Consumption of TH8321WF Thermostat:

Backlight on: 2.35 VA

Backlight off: 1.40 VA

Wi-Fi Communication Requirements:

802.11 b/g/n routers

Android or IOS Smartphone, tablet or device

Temperature Setting Range:

Heating: 40 to 90 °F (4.5 to 32 °C)

Cooling: 50 to 99 °F (10 to 37 °C)

Temperature Sensor Accuracy:

± 1.5 °F at 70 °F (0.75 °C at 21.0 °C)

Humidification Setting Range: 10% to 60% RH

Dehumidification Setting Range: 40% to 80% RH

Humidity Display Range: 0% to 99%

Humidity Sensor Accuracy:

± 5% RH from 30% to 50% RH at 75 °F (24 °C)

Cool Indication:

Displays "Cool On" when the thermostat turns the cooling on.

Heat Indication:

Displays "Heat On" when the thermostat turns the heating on.

Auxiliary Heat Indication:

Displays "Aux Heat On" when the thermostat turns the auxiliary heat on.

Interstage Differential:

Comfort: The thermostat keeps the indoor temperature within 1 degree of the setpoint (droop less control). The thermostat turns on stage 2 when the capacity on stage 1 reaches 90%.

When the interstage differential is set to 1.0 or higher, the thermostat stages the equipment based on how far the indoor temperature is from the setpoint.

Clock Accuracy:

If not connected to Wi-Fi: 1 minute per month at 77 °F (25 °C). ± 2 minutes per month over the operating ambient temperature range.

If connected to Wi-Fi and registered to Total Connect Comfort: the current time is synced via the Internet.

Mounting Means:

Thermostat mounts directly on the wall in the living space using mounting screws and anchors provided. Fits a horizontal 2 x 4 in. junction box. Use a cover plate and its mounting bracket to mount the thermostat onto a vertical 2 x 4 in. junction box.

Job Name _____

Engineer _____

Mechanical Contractor _____

Contractor's P.O. No. _____

Representative _____

Notes _____

Model(s)
 TH8321WF1001 Qty. _____ Notes _____

Approval _____

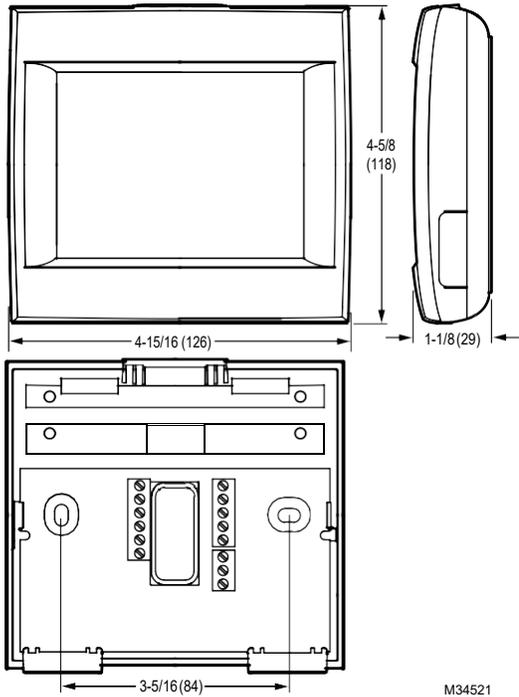
Service _____

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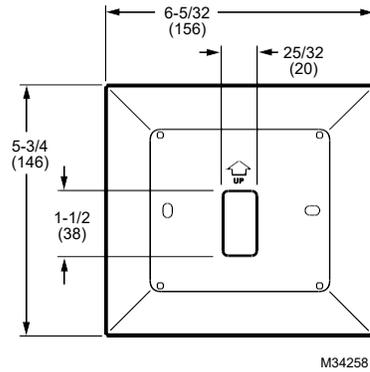


Product	Part Number	Operating Ambient Temperature	Operating Relative Humidity	Shipping Temperature	Physical Dimensions in in. (mm)	Color(s)
Thermostat	TH8321WF1001	32 to 120 °F (0 to 48.9 °C)	5% to 90% Non-Condensing	-20 to 120 °F (-28.9 to 48.9 °C)	4-15/16 x 4-5/8 x 1-1/8 (126 x 118 x 29)	Arctic White

Dimensions of thermostat in in. (mm).



Dimensions of VisionPRO cover plate in in. (mm).



Job Name:

System Reference:

Date:

Indoor Unit:
PVA-A36AA7



Outdoor Unit:
PUZ-HA36NHA5



INDOOR UNIT FEATURES

- Ducted air handler provides a solution to cool and heat large zones
- Highly efficient totally enclosed ECM motor
- Selectable external static pressure: 0.30, 0.50 and 0.80 in.WG with 3 fan speeds at each static setting
- 1 inch R4.2 fiberglass free insulation reduces condensation and boosts efficiency
- Positive pressure cabinet with air leakage of less than 1.0% at 1.0 in.WG
- Unique blow through design allows simple coil cleaning when the blower is removed
- Multi-position installation: horizontal (left or right), vertical (up or down). For downflow configurations, the CMA-1 is recommended for proper management of condensate to prevent water blow-off in certain conditions
- Optional electric heat kit for additional heat capacity
- Optional humidifier control and ERV control

OUTDOOR UNIT FEATURES

- Variable speed INVERTER-driven compressor
- High heating capacity: flash injection circuit maintains 100% heating capacity at 5°F outdoor temperature
- Wide heating range: heating performance down to -13°F (average of 80% heating capacity)
- High speed heating at start up: Hyper-Heating INVERTER® reduces the time for heating at start up by about half compared to standard models
- Suction accumulator pre-charged with refrigerant volume for piping length up to 100 ft.
- Twinning of two indoor units possible with the 36 kBtu/h model
- High pressure/temperature protection

SPECIFICATIONS: PVA-A36AA7 & PUZ-HA36NHA5

Model Number	Indoor Unit		PVA-A36AA7
	Outdoor Unit		PUZ-HA36NHA5
Cooling ¹	Maximum Capacity	Btu/h	36,000
	Rated Capacity	Btu/h	33,000
	Minimum Capacity	Btu/h	18,000
	Maximum Power Input	W	3,040
	Rated Power Input	W	2,640
	Moisture Removal	Pints/h	7.4
	Sensible Heat Factor		0.74
	Power Factor	%	87.6
Heating at 47°F ²	Maximum Capacity	Btu/h	40,000
	Rated Capacity	Btu/h	38,000
	Minimum Capacity	Btu/h	18,000
	Maximum Power Input	W	3,360
	Rated Power Input	W	3,040
	Power Factor	%	88.7
Heating at 17°F ³	Maximum Capacity	Btu/h	38,000
	Rated Capacity	Btu/h	29,000
	Maximum Power Input	W	5,400
	Rated Power Input	W	3,230
Heating at 5°F ⁴	Maximum Capacity	Btu/h	38,000
	Maximum Power Input	W	6,100
Efficiency	SEER		17.8
	EER ¹		12.5
	HSPF (IV)		11.0
	COP at 47°F ²		3.66
	COP at 17°F in Maximum Capacity		2.06
	COP at 5°F in Maximum Capacity		1.82
	ENERGY STAR® Certified (ENERGY STAR products are third-party certified by an EPA-recognized Certification Body)		Yes
Electrical	Voltage, Phase, Frequency		208 / 230V, 1-phase, 60 Hz
	Guaranteed Voltage Range	V AC	198 – 253
	Voltage: Indoor - Outdoor, S1-S2	V AC	208V / 230
	Voltage: Indoor - Outdoor, S2-S3	V DC	24
	Voltage: Indoor - Remote controller	V DC	12
	Recommended Fuse/Breaker Size	A	30
	Recommended Wire Size (Indoor - Outdoor)	AWG	14
Indoor Unit	MCA	A	5.50
	Fan Motor Full Load Amperage	A	4.40
	Fan Motor Output	W	430
	Airflow Rate, Dry	CFM	788-956-1125

SPECIFICATIONS: PVA-A36AA7 & PUZ-HA36NHA5

Model Number	Indoor Unit		PVA-A36AA7
	Outdoor Unit		PUZ-HA36NHA5
	Airflow Rate, Wet	CFM	n/a
	External Static Pressure	in.WG	0.30-0.50-0.80
	Sound Pressure Level	dB(A)	30-34-38
	Drain Pipe Size	In. (mm)	3/4 FPT (19.05)
	Condensate Lift Mechanism, Maximum Distance	Ft. (m)	n/a
	Heat Exchanger Type		Plate fin coil
	External Finish Color		Galvanized steel cabinet-Powder coated Slate Gray
	Unit Dimensions // Grille Dimensions	W: In. (mm)	25 (635)
		D: In. (mm)	21-5/8 (548)
		H: In. (mm)	59-1/2 (1511)
Unit Weight	Lbs. (kg)	172 (78)	
Indoor Unit Operating Temperature Range	Cooling Intake Air Temp (Maximum / Minimum)	°F	90 DB, 73 WB / 66 DB, 59 WB
	Heating Intake Air Temp (Maximum / Minimum)	°F	82 DB / 50 DB
Outdoor Unit	MCA	A	28
	MOCP	A	40
	Fan Motor Full Load Amperage	A	0.4+0.4
	Fan Motor Output	W	86+86
	Airflow Rate	CFM	3,530
	Refrigerant Control		Electronic Expansion Valve
	Defrost Method		Reverse Cycle
	Heat Exchanger Type		Cross fin
	Sound Pressure Level, Cooling ¹	dB(A)	52
	Sound Pressure Level, Heating ²	dB(A)	53
	Compressor Type		INVERTER-Driven Twin Rotary
	Compressor Model		ANB33FJEMT
	Compressor Rated Load Amps	A	18
	Compressor Locked Rotor Amps	A	27.5
	Compressor Oil Type // Charge	oz.	FV50S // 45
	External Finish Color		Ivory Munsell 3Y 7.8/1.1
	Base Pan Heater		n/a
	Unit Dimensions	W: In. (mm)	37-3/8 (950)
		D: In. (mm)	13 + 1-3/16 (330 + 30)
		H: In. (mm)	53-1/8 (1,350)
Package Dimensions	W: In. (mm)	40-15/16 (1,040)	
	D: In. (mm)	17-11/16 (450)	
	H: In. (mm)	56-11/16 (1,440)	
Unit Weight	Lbs. (kg)	265 (120)	
Package Weight	Lbs. (kg)	289 (131)	

SPECIFICATIONS: PVA-A36AA7 & PUZ-HA36NHA5

Model Number	Indoor Unit		PVA-A36AA7
	Outdoor Unit		PUZ-HA36NHA5
Outdoor Unit Operating Temperature Range	Cooling Intake Air Temp (Maximum / Minimum)	°F	115 DB / 0* DB
	Heating Intake Air Temp (Maximum / Minimum)	°F	70 DB, 59 WB / -13 DB, -13 WB
	Thermal Lock-out / Re-start Temperatures**	°F	n/a
Refrigerant	Type		R410A
	Charge	Lbs, oz	12
Piping	Gas Pipe Size O.D. (Flared)	In.(mm)	5/8 (15.88)
	Liquid Pipe Size O.D. (Flared)	In.(mm)	3/8 (9.52)
	Maximum Piping Length	Ft. (m)	245 (75)
	Maximum Height Difference	Ft. (m)	100 (30)
	Maximum Number of Bends		15

Notes

AHRI Rated Conditions (Rated data is determined at a fixed compressor speed)	¹ Cooling (Indoor // Outdoor)	°F	80 DB, 67 WB // 95 DB, 75 WB
	² Heating at 47°F (Indoor // Outdoor)	°F	70 DB, 60 WB // 47 DB, 43 WB
	³ Heating at 17°F (Indoor // Outdoor)	°F	70 DB, 60 WB // 17 DB, 15 WB
Conditions	⁴ Heating at 5°F (Indoor // Outdoor)	°F	70 DB, 60 WB // -4 DB, -5 WB

*Wind baffles required to operate below 23°F DB in cooling mode. PUZ with wind baffle: 0°F - 115°F.
**System cuts out in heating mode to avoid thermistor error and automatically restarts at these temperatures.

ACCESSORIES: PVA-A36AA7

Signal Receiver	□ PAR-SA9CA-E
Wireless Remote Controller	□ PAR-FL32MA-E
Wireless Remote Receiver	□ PAR-FA32MA-E
Backlit, Wall-mounted, Wireless Controller	□ MHK1
Portable Central Controller	□ MCCH1
Wired MA Controller	□ PAR-33MAA
Simple MA Controller	□ PAC-YT53CRAU
Touch MA Controller	□ PAR-CT01MAU-SB
Wired Remote Sensor	□ PAC-SE41TS-E
Wireless Temperature and Humidity Sensor	□ PAC-USWHS003-TH-1
Outside Air Sensor for MHK1	□ MOS1
Wireless Interface	□ PAC-USWHS002-WF-1
Thermostat Interface	□ PAC-US444CN-1
kumo station®	□ PAC-WHS01HC-E
USNAP Interface	□ PAC-WHS01UP-E
IT Extender	□ PAC-WHS01IE-E
BACnet® and Modbus Interface	□ PAC-UKPRC001-CN-1
External Fan / Heater Control Relay Adapter	□ CN24RELAY-KIT-CM3
Connector cable for remote display	□ PAC-SA88HA-EP
Connector for CN32 (remote on/off)	□ PAC-SE55RA-E
Remote Operation Adapter (with wire terminals for remote ON/OFF and operation status/ error) ¹	□ PAC-SF40RM-E
Blue Diamond Sensor Extension Cable—15 Ft.	□ C13-103
MegaBlue Advanced Blue Diamond Condensate Pump w/ Reservoir & Sensor	□ X87-835 - 110 to 250V
MaxiBlue Advanced Blue Diamond Mini Condensate Pump w/ Reservoir & Sensor (208/230V) up to 48,000 Btu/h [recommended]	□ X87-721 - 208/230V
MegaBlue Blue Diamond Condensate Pump (110-230V) up to 170,000 Btu/h	□ X87-835
Drain Pan Level Sensor (Control for indoor unit shut off to prevent drain pan overflow)	□ DPLS2
3 Pole Disconnect Switch (30A/600VUL) [fits 2"X4" utility] - Black	□ TAZ-MS303
Separate Power Terminal Block Kit	□ SPTB1
Electric Heat Lockout Control	□ ETC-211000-MIT
Electric Heat Kit for Multi-position AHU	□ EH10-MPA-L(B)
Electric Heat Kit for Multi-position AHU	□ EH15-MPAS- L(B)

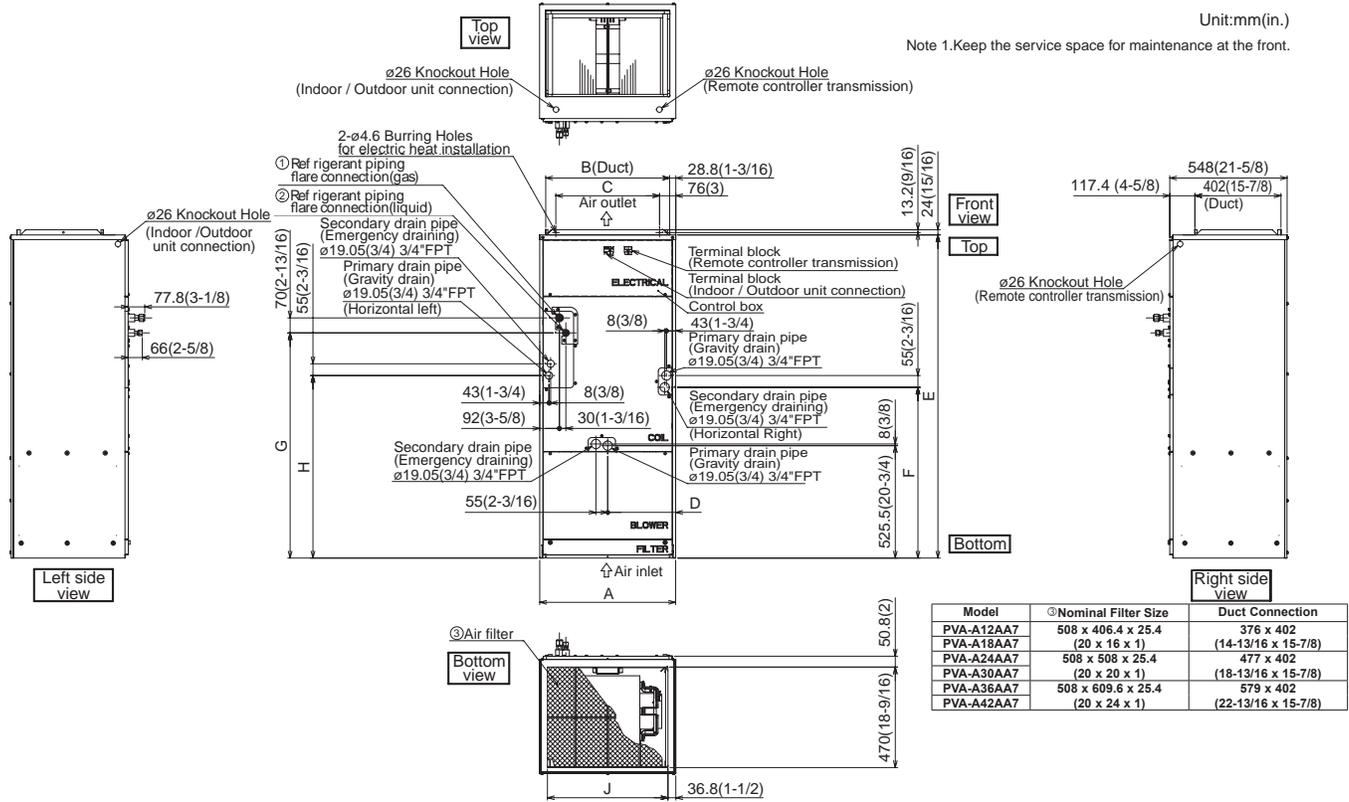
¹ Unable to use with wireless remote controller

ACCESSORIES: PUZ-HA36NHA5

Air Outlet Guide	□ PAC-SG59SG-E
Front Wind Baffle	□ WB-PA5
Drain Socket	□ PAC-SG61DS-E
Centralized Drain Pan	□ PAC-SG63DP-E
M-NET Converter	□ PAC-SF83MA-E
M-NET Converter	□ PAC-SJ95MA-E
Control/Service Tool	□ PAC-SK52ST
Hail Guard	□ HG-A2
Condensing Unit Mounting Pad 24" x 42" x 3"	□ ULTRILITE2
Outdoor Unit Stand—12" High	□ QSMS1202M
Outdoor Unit Stand—18" High	□ QSMS1802M
Outdoor Unit Stand—24"High	□ QSMS2402M
Heavy Duty Wall Mounting Bracket for Outdoor Units—Coated Steel	□ QSWB2000M-1
Heavy Duty Wall Mounting Bracket for Outdoor Units—316 Series Stainless Steel	□ QSWBSS
3/8" x 5/8" x 10' / 1/2" Lineset (Twin-Tube Insulation)	□ MPLS385812T-10
3/8" x 5/8" x 15' / 1/2" Lineset (Twin-Tube Insulation)	□ MPLS385812T-15
3/8" x 5/8" x 30' / 1/2" Lineset (Twin-Tube Insulation)	□ MPLS385812T-30
3/8" x 5/8" x 50' / 1/2" Lineset (Twin-Tube Insulation)	□ MPLS385812T-50
3/8" x 5/8" x 65' / 1/2" Lineset (Twin-Tube Insulation)	□ MPLS385812T-65
3/8" x 5/8" x 100' / 1/2" Lineset (Twin-Tube Insulation)	□ MPLS385812T-100

DIMENSIONS: PVA-A36AA7 & PUZ-HA36NHA5

PVA-A36AA7



Model	⊙Nominal Filter Size	Duct Connection
PVA-A12AA7	508 x 406.4 x 25.4 (20 x 16 x 1)	376 x 402 (14-13/16 x 15-7/8)
PVA-A18AA7	508 x 508 x 25.4 (20 x 20 x 1)	477 x 402 (18-13/16 x 15-7/8)
PVA-A24AA7	508 x 609.6 x 25.4 (20 x 24 x 1)	579 x 402 (22-13/16 x 15-7/8)

Model	A	B	C	D	E	F	G	H	J	Unit: mm (in.)	
										⊙Gas Pipe	⊙Liquid Pipe
PVA-A12AA7	432 (17)	376 (14-13/16)	281 (11-1/8)	224 (8-7/8)	1275 (50-1/4)	680 (26-13/16)	823 (32-7/16)	735.5 (29)	360 (14-3/16)	Φ 12.7 (1/2)	Φ 6.35 (1/4)
PVA-A18AA7	534 (21)	477 (18-13/16)	382.6 (15-1/8)	266.5 (10-1/2)	1378 (54-1/4)	737 (29-1/16)	953.5 (37-9/16)	792 (31-3/16)	461 (18-3/16)	Φ 15.88 (5/8)	Φ 9.52 (3/8)
PVA-A24AA7	635 (25)	579 (22-13/16)	484.6 (19-1/8)	317.5 (12-1/2)	1511 (59-1/2)	798.5 (31-7/16)	1053 (41-1/2)	853.5 (33-5/8)	563 (22-3/16)	Φ 15.88 (5/8)	Φ 9.52 (3/8)

NRK 0150-0700

Reversible air/water heat pump

Cooling capacity 8.8 - 148 ton
Heating capacity 116,866 - 593,235 BTU/W

- Production of hot water down to 149 °F
- Heating operations with external temperatures down to - 4 °F
- Optimized for operation in heating mode
- High efficiency also at partial loads
- Night mode



DESCRIPTION

Reversible air/water heat pump for air conditioning systems with cold water production for cooling rooms and hot water for heating and/or domestic hot water services, suitable for connection in residential, commercial complexes or industrial applications.

It's optimised for use in heating mode, and can be combined not only with low-temperature emission systems such as floor heating or fan coils, but also conventional radiators.

Equipped with inverter compressors, axial fans, external coil with aluminium fins, plate heat exchanger on the side.

The base the structure and the panels are made of steel treated with polyester paint RAL 9003.

VERSIONS

A High efficiency

FEATURES

Operating field

Working at full load down to - 4 °F outside air temperature in winter, and down to 118.4 °F in summer. Hot water production down to 149 °F.

Version with Integrated hydronic kit

Integrated hydronic kit containing the main hydraulic components; available with various configurations to obtain a solution that allows you to facilitate installation.

Inverter fans

Standard inverter fans for all size.

CONTROL

Microprocessor adjustment, with keyboard and LCD display, for easy access on the unit is a menu available in several languages.

Adjustment includes complete management of the alarms and their log.

The presence of a programmable timer allows functioning time periods and a possible second set-point to be set.

The temperature control takes place with the inte-gral proportional logic, based on the water output temperature.

NIGHT MODE

It is possible to set a silenced operation profile. Perfect for night operation since it guarantees greater acoustic comfort in the evenings, and a high efficiency in the time of greater load.

■ Available for all units with inverter fans.

ACCESSORIES

AER485P1: RS-485 interface for supervision systems with MODBUS protocol.

AERNET: The device allows the control, the management and the remote monitoring of a Chiller with a PC, smartphone or tablet using Cloud connection. AERNET works as Master while every unit connected is configured as Slave (max. 6 unit); also, with a simple click is possible to save a log file with all the connected unit datas in the personal terminal for post analysis.

CRATE02: Special crate for transport

CRATE03: Special crate for transport

MODU-485BL: RS-485 interface for supervision systems with MODBUS protocol.

MULTICHILLER_EVO: Control, switch-on and switch-off system of the single chillers where multiple units are installed in parallel, always ensuring constant flow rate to the evaporators.

PGD1: Allows you to control the unit at a distance.

GP: Anti-intrusion grid.

VT: Antivibration supports

FACTORY FITTED ACCESSORIES

DRE: Electronic device for peak current reduction.

RIF: Power factor correction. Connected in parallel to the motor allowing about 10% reduction of input current.

RESNRK: Electric heater for the control and electric power board.

ACCESSORIES COMPATIBILITY

Accessories

Model	Ver	0150	0300	0330	0350	0550	0600	0650	0700
AER485P1	A		*	*	*	*	*	*	*
AERNET	A	*	*	*	*	*	*	*	*
CRATE02	A		*	*	*	*			
CRATE03	A						*	*	*
MODU-485BL	A	*							
MULTICHILLER_EVO	A		*	*	*	*	*	*	*
PGD1	A		*	*	*	*	*	*	*

Anti-intrusion grid

Ver	0150	0300	0330	0350	0550	0600	0650	0700
A	-	GP2 x 2 (1)	GP2 x 3 (1)	GP2 x 3 (1)	GP2 x 3 (1)			

(1) x _ indicates the quantity to buy.

The accessory cannot be fitted on the configurations indicated with -

Antivibration

Ver	0150	0300	0330	0350	0550	0600	0650	0700
Integrated hydronic kit: 00, 01, 03, P1, P3								
A	VT15	-	-	-	-	-	-	-

The accessory cannot be fitted on the configurations indicated with -

Device for peak current reduction

Ver	0150	0300	0330	0350	0550	0600	0650	0700
A	-	DRENK03007	DRENK03307	DRENK35557	DRENK35557	DRENK60657	DRENK60657	DRENK07007

The accessory cannot be fitted on the configurations indicated with -

A grey background indicates the accessory must be assembled in the factory

Power factor correction

Ver	0150	0300	0330	0350	0550	0600	0650	0700
A	-	RIFNRK03007	RIFNRK03307	RIFNRK35557	RIFNRK35557	RIFNRK60657	RIFNRK60657	RIFNRK07007

The accessory cannot be fitted on the configurations indicated with -

A grey background indicates the accessory must be assembled in the factory

Electric heater for the control and electric power board

Ver	0150	0300	0330	0350	0550	0600	0650	0700
A	-	RESNRK03007	RESNRK33707	RESNRK33707	RESNRK33707	RESNRK33707	RESNRK33707	RESNRK33707

The accessory cannot be fitted on the configurations indicated with -

A grey background indicates the accessory must be assembled in the factory

CONFIGURATOR

Field	Description
1,2,3	NRK
4,5,6,7	Size 0150, 0300, 0330, 0350, 0550, 0600, 0650, 0700
8	Operating field
°	Standard mechanic thermostatic valve (1)
9	Model
H	Heat pump
10	Heat recovery
°	Without heat recovery
D	With desuperheater (2)
11	Version
A	High efficiency
12	Coils
°	Rame - alluminio
R	Copper-copper
S	Copper-Tinned copper
13	Fans
J	EC Inverter type
14	Power supply
7	460YV 3 ~ 60Hz
15,16	Integrated hydronic kit (3)
00	Without hydronic kit
01	Storage tank with low head pump
02	Storage tank with low head pump + stand-by pump
03	Storage tank with high head pump
04	Storage tank with high head pump + stand-by pump
P1	Single pump low head
P2	Pump low head + stand-by pump
P3	Single pump high head
P4	Pump high head + stand-by pump

(1) Water produced down to +39.2 °F

(2) The desuperheater must be isolated in heating mode. In cooling mode, a water temperature no lower than 95°F must always be guaranteed on the heat exchanger inlet.

(3) Option available only for size 0150

PERFORMANCE SPECIFICATIONS

NRK - (A) / 54.1/44.1 °C - 104 °F/113 °F

Size		0150	0300	0330	0350	0550	0600	0650	0700
Cooling performance 54.1 °F / 44.1 °F (1)									
Cooling capacity	ton	8.8	16.1	19.0	21.5	24.0	32.3	36.6	39.7
Input power	kW	9.6	20.2	23.7	27.0	29.9	40.3	49.9	58.1
EER	BTU/W	11.02	9.55	9.61	9.56	9.61	9.63	8.81	8.19
IPLV	BTU/W	14.91	13.51	13.58	13.41	13.38	13.79	12.73	11.23
Water flow rate system side	gpm	21.1	38.5	45.4	51.5	57.4	77.3	87.6	94.9
Pressure drop system side	ft H ₂ O	17.81	5.69	5.69	5.69	5.69	5.69	5.69	5.69
Heating performance 104 °F / 113 °F (2)									
Heating capacity	BTU/h	116,866	231,872	275,841	304,206	340,426	463,802	539,671	593,235
Input power	kW	10.0	21.0	26.4	29.2	31.9	43.4	51.3	57.2
COP	kW/kW	3.41	3.24	3.06	3.05	3.13	3.13	3.08	3.04
Water flow rate system side	gpm	26.2	52.0	61.9	68.2	76.3	104.0	121.0	133.0
Pressure drop system side	ft H ₂ O	27.39	10.42	10.59	10.01	10.09	10.31	10.87	11.19

(1) Data: System side water heat exchanger 54.1 °F / 44.1 °F; External air 95 °F

(2) Data: System side water heat exchanger 104 °F / 113 °F; External air 44.6 °F

PARTIALISATIONS EER

Size		0150	0300	0330	0350	0550	0600	0650	0700
Partialisations EER									
100 %	BTU/W	11.02	9.55	9.62	9.55	9.62	9.62	8.80	8.19
75 %	BTU/W	13.38	12.01	12.01	11.94	11.98	12.83	11.81	10.58
50 %	BTU/W	15.80	14.40	14.47	14.26	14.19	14.77	13.65	11.98
25 %	BTU/W	17.20	15.63	16.17	15.66	15.49	13.79	12.76	10.99

ELECTRIC DATA

Size		0150	0300	0330	0350	0550	0600	0650	0700
Electric data									
Peak current (LRA)	A	133.6	165.3	184.0	222.0	222.9	198.6	234.1	278.4
Minimum circuit amperage (MCA)	A	30	59	57	72	71	88	103	123
Maximum overcurrent permitted by the protection device (MOP)	A	47	76	78	97	96	105	124	148

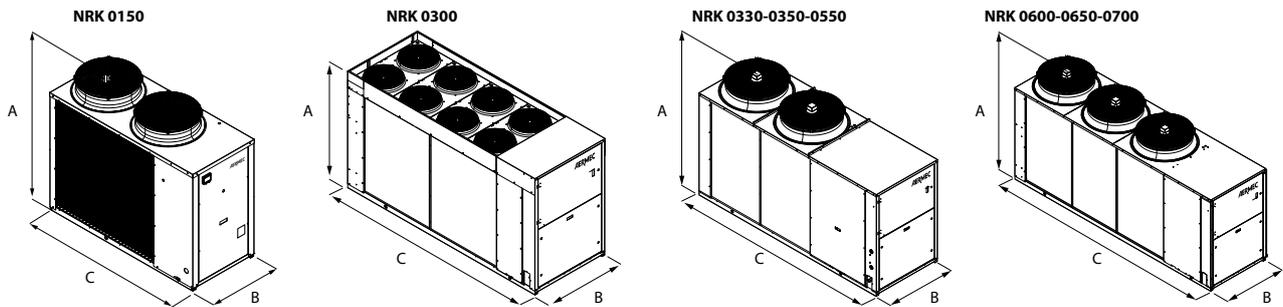
GENERAL TECHNICAL DATA

Size			0150	0300	0330	0350	0550	0600	0650	0700
Compressor										
Type	A	type	Scroll							
Compressor regulation	A	Type	On-Off							
Number	A	no.	1	2	2	2	2	4	4	4
Circuits	A	no.	1	2	2	2	2	2	2	2
Refrigerant	A	type	R410A							
System side heat exchanger										
Type	A	type	Braze plate							
Number	A	no.	1	1	1	1	1	1	1	1
System side hydraulic connections										
Connections (in/out)	A	Type	Gas - F	Grooved joints						
Sizes (in/out)	A	Ø	1"1/4	2"1/2 US						
Inverter fan										
Type	A	type	Axial							
Fan motor	A	type	EC Inverter motors							
Number	A	no.	2	8	2	2	2	3	3	3
Air flow rate	A	cfm	8,064	23,190	22,366	21,954	21,954	33,314	37,904	37,904
Sound data calculated in cooling mode										
Sound power (1)	A	dB(A)	82.9	85.4	85.4	92.3	86.2	88.1	87.8	95.2
Sound pressure level (10 m/33ft) (2)	A	dB(A)	51.3	53.6	53.5	60.4	54.3	56.1	55.7	63.1

(1) Sound power calculated on the basis of measurements made in accordance with UNI EN ISO 9614-2, as required for Eurovent certification.

(2) Sound pressure (cold functioning) measured in free field, 10m/33ft away from the unit external surface (in compliance with UNI EN ISO 3744).

DIMENSIONS



Size		0150	0300	0330	0350	0550	0600	0650	0700
Dimensions and weights for transport									
A	in	62.3	63.3	73.9	73.9	73.9	73.9	73.9	73.9
B	in	72.9	128.1	131.2	131.2	131.2	170.6	170.6	170.6
C	in	34.3	43.3	43.3	43.3	43.3	43.3	43.3	43.3
Dimensions and weights									
Weight empty	lb	820	1,729	1,846	1,938	1,955	2,544	2,544	2,596
Weight functioning	lb	833	1,742	1,862	1,958	1,976	2,572	2,572	2,626

Aermec reserves the right to make any modifications deemed necessary.
All data is subject to change without notice. Aermec does not assume responsibility or liability for errors or omissions.

Aermec S.p.A.

Via Roma, 996 - 37040 Bevilacqua (VR) - Italia
Tel. 0442633111 - Telefax 044293577
www.aermec.com



Chilmark School



HVAC Engineering Services

December 6, 2019

The Up Island Regional School Committee & the Town of Chilmark are seeking proposals from qualified engineers to provide the services necessary to accomplish the following:

I. Current Needs

A. School needs a reliable, efficient, & effective heating system for the 11,000 sq foot, 13 room building housing Preschool – 5th Grade with 55 k-5 and 16 pre-k students.

1. The school is considering a Cold Climate Heat Pump HVAC system to replace or augment the existing systems to improve comfort in the building and achieve Green Community status.
2. The school thinks it would like to complete upgrades to the existing oil fired boiler system, if it is retained in any manner.
3. The school is concerned that the attic spaces may need to receive additional insulation.
4. The school desires an upgraded control system that is controllable in the classrooms, through a main control, and remotely.
5. The School would like to ensure that the fire suppression system (sprinkler heads) has not been compromised by recent or future changes to the HVAC system.
6. The school expects to need an appropriately sized back-up power generator if Cold Climate Heat Pumps are installed.
7. Recently installed ERV units in classrooms are considered noisy and circulate cool air during the winter. The School would like to explore a solution to these complaints, possibly moving the ERVs to the attic spaces or re-purposing the original air handling units in the attic spaces.

II. Engineer would provide a comprehensive approach to responsive needs listed above

1.
 - a) The engineer will assess the existing HVAC system.
 - b) The engineer will review the potential solutions to the current HVAC concerns.
 - c) The engineer will provide options for the School to consider
2. Options recommended by the engineer will take into consideration all normal industry standards, with special focus on

- Building & Occupant Health
- Installation cost
- Operating cycles
- Operating costs
- Environmental Impact/Energy Efficiency

III. Existing Systems

The building was constructed in 1998.

It was fitted with a two boiler system that provided domestic hot water to hand washing sinks in classroom, hot water to baseboard radiators, and hot water to heat exchangers in six (6) attic mounted air handing units for forced hot air and to heat fresh air for the classrooms. The boilers ran separately and together to meet the design load for the building. This system was sufficient to the comfort needs of the occupants.

Several non-boiler system building issues came up that resulted in water damage from frozen pipes in the domestic water and fire suppression system.

The “flat roof” areas over the hallways received remedial thermal treatment with spray foam insulation after domestic water lines froze and leaked through the ceilings.

The Air Handlers in the uninsulated and ventilated attics were wrapped in insulation after (the rooves were designed as “air washed”) after the cold outside air caused one unit to go into “survival mode” during particularly cold weather, and a poorly installed section of the fire suppression system piping froze and burst flooding the classroom. Ceilings of classrooms also received additional insulation.

The Control system was modified at some point since construction when the PC controlled thermostats and outdated software/hardware were failing.

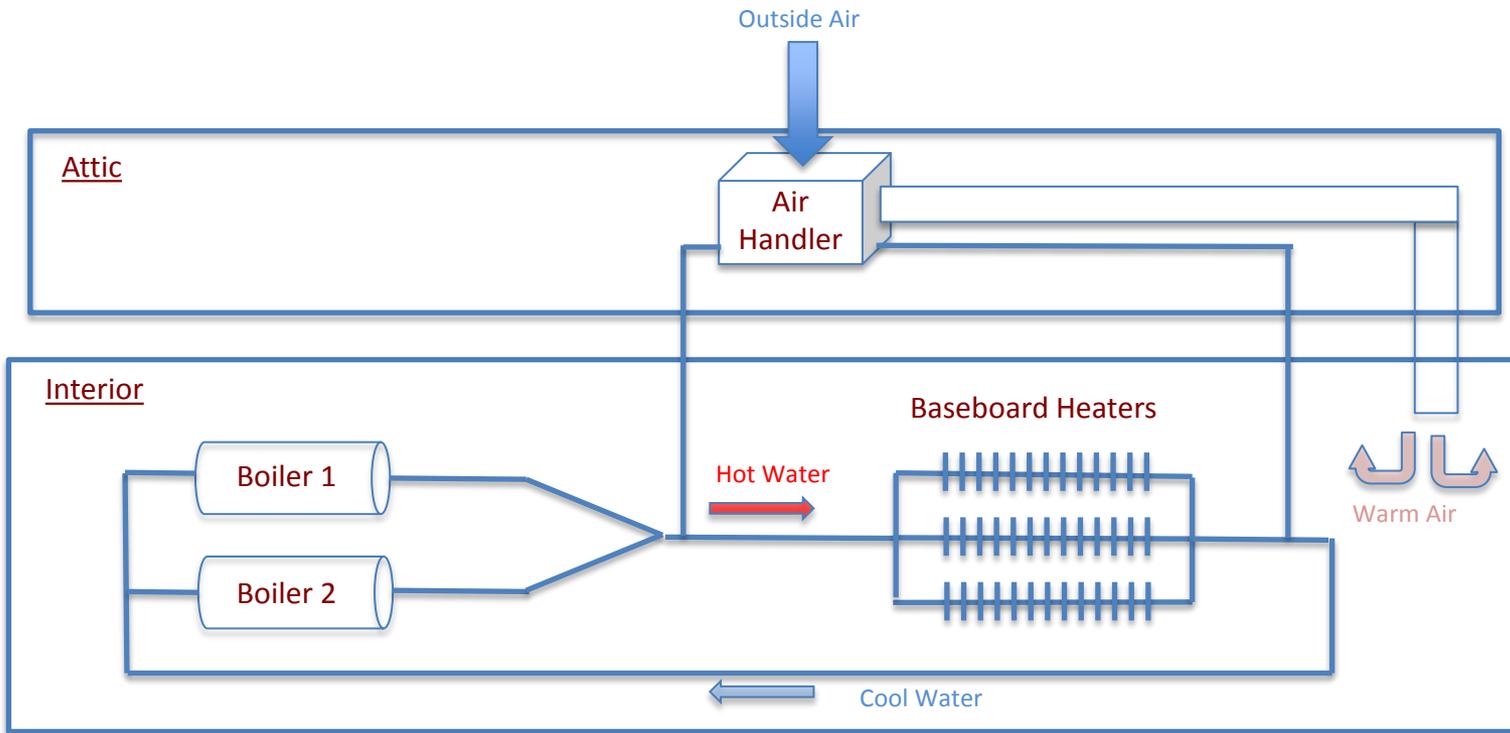
One of the two boilers has now failed. It was being replaced this summer, when the school decided to stop and consider the installation of non-fossil fuel heating. We are running successfully on one boiler at this time.

When the ERVs were installed into the classrooms, the air handlers were disabled. We don’t know how they were disabled or if they were fully decommissioned in place.

With the disabling of the air handlers the classrooms stopped receiving heat from the forced hot air ceiling vents. This left some rooms colder as linear feet of baseboard covers was not all radiators. The installation of a donation “mini-split” in one classroom has made the room usable in the cold months again.

PROPOSALS should be sent to: DEADLINE is December 16, 2019 @ 5:00 PM
Town Administrator, PO Box 119, 401 Middle Road, Chilmark, MA 02535

QUESTIONS: Tim Carroll townadministrator@chilmarkma.gov 508-645-2101



Original Design

Heating with dual oil-fired boilers
 Ventilation system poorly designed and located
 AC non-existent

Needed Work

Appropriate insulation of attic space
 Heat pump heating with 1 boiler as backup
 Controls
 Noise mitigation for classrooms

ROOM	Area, ft2	FTR 1	BTU/hr/ft at 190F average water temperature						BTU/hr per CUH				Total	BTU/hr/ft2
			1800		950		1320		9700		40000			
			BTU/hr	FTR 2	BTU/hr	FTR 3	BTU/hr	CUH 2,3,4	CUH 1,5,6,7,8	CUH 1,5,6,7,8				
Classroom 133	935	12	21600						1	9700			31300	33
Special Ed 132	160	3	5400										5400	34
Classroom 130	938	16	28800										28800	31
Classroom 126 Tech	677	12	21600										21600	32
Classroom 123 Art/Music	631	10	18000										18000	29
Reception 111	174	4	7200										7200	41
Lobby 110	890													
Hallways 127, 128, 129	1689			38	36100						5	200000	236100	92
Principal 117	136	4	7200										7200	53
Conference 118	156												0	0
Nurse 119	88												0	0
Entry adjacent Kindergarten	94						4	5280					5280	
Kindergarten 121	1082	12	21600						1	9700			31300	29
Classroom 131	942	16	28800										28800	31
Meeting 135	167	3	5400										5400	32
Classroom 134	942	12	21600						1	9700			31300	33

9701

Total @ 190F AWT 457,680 BTU/hr
Estimated Total @ 170F AWT 366,144 BTU/hr

CERTIFICATE OF INSPECTION
BOILER or PRESSURE VESSEL

Located at:
Chilmark Elementary School
8 State Road
Chilmark, MA 02535-1433

Owner or User:
Town of Chilmark
401 Middle Road
Chilmark, MA 02535-1995

Type Tag Number
CI **MA196835**

Pressure not to exceed
87 **lbs/sq. in.**

NB# Manufacturer
 Buderus

Expiration Date : **Jun-2019**

Plant Loc: **Boiler Room**

THE COMMONWEALTH OF
MASSACHUSETTS
DEPARTMENT OF FIRE SERVICES
BPV
One State Rd.
Stow, MA 01775-1025



This is to certify that the boiler or pressure vessel herein has been inspected and approved for use in accordance with the provisions of M.G.L. Chapter 146.

Notify this department at once if any defect is discovered.
POST UNDER GLASS IN CONSPICUOUS PLACE IN ENGINE OR BOILER ROOM OR NEXT TO PRESSURE VESSEL.

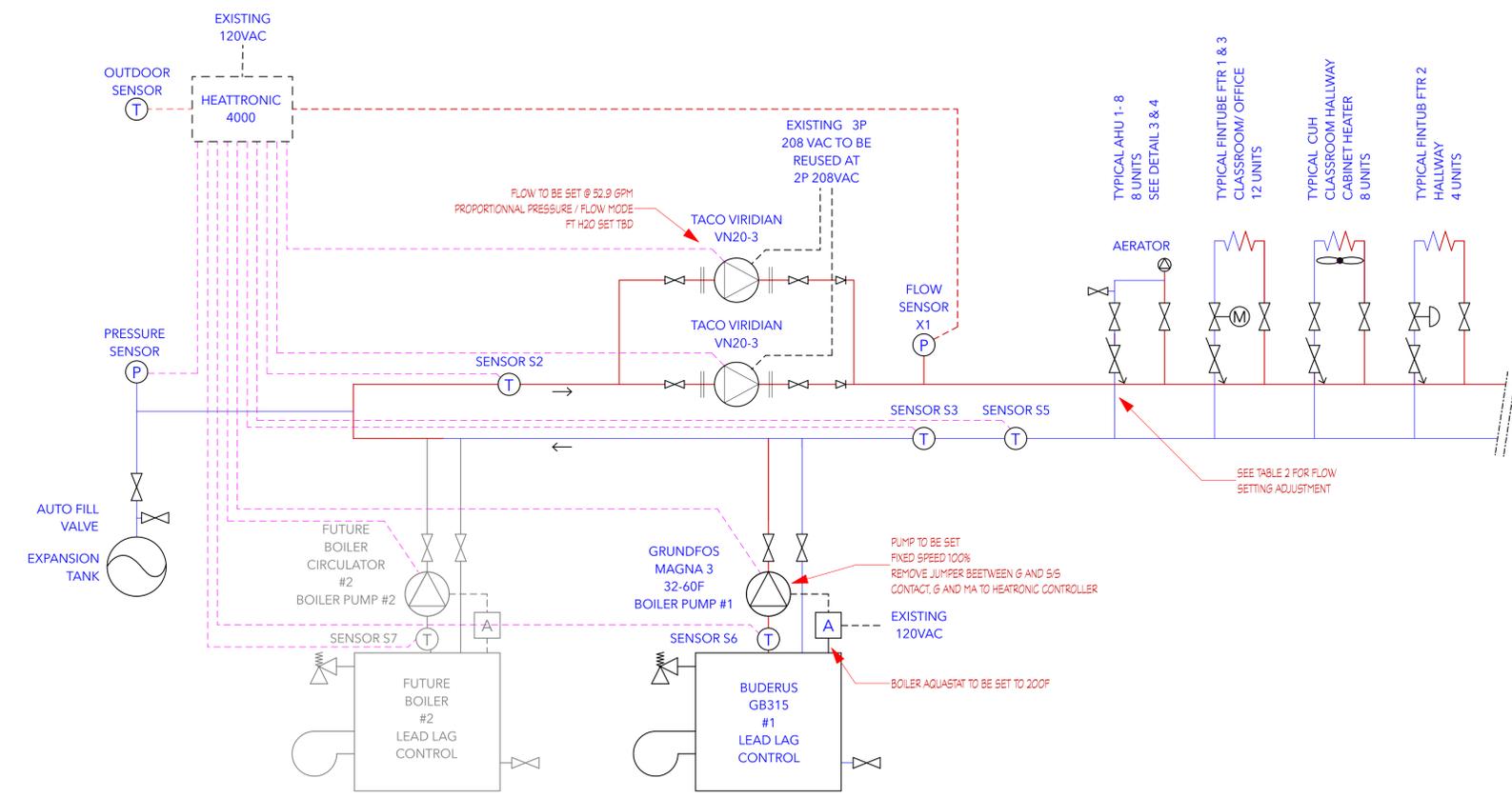
Christopher Hastings

Travelers

A handwritten signature in black ink, appearing to read "Peter J. Ostroskey".

Peter J. Ostroskey
State Fire Marshal

	RETURN
	SUPPLY
	AUTOMATIC AIR VENT
	LOW VOLTAGE SENSOR
	THERMOMETER
	DIVERTING VALVE
	EXPANSION TANK
	CIRCULATOR
	MOTORIZED ZONE VALVE
	FLOW BALANCING VALVE
	NON ELECTRIC THERMOSTATIC VALVE
	1/4 TURN VALVE
	PRESSURE RELIEF VALVE
	LOW VOLTAGE WIRING
	LINE VOLTAGE WIRING
	EXISTING LOW VOLTAGE WIRING
	AQUASTAT CONTROL



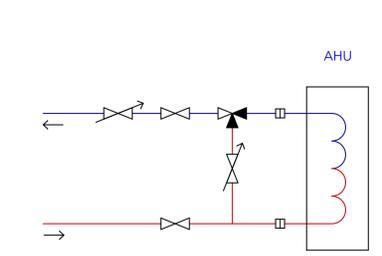
NOTE: THIS SCHEMATIC IS NOT AN AS BUILT DRAWING OF THE SYSTEM AND THEREFORE SOME COMPONENTS MIGHT NOT BE ACCURATELY DRAWN.

1 BOILER ROOM PIPING AND CONTROL SCHEMATIC

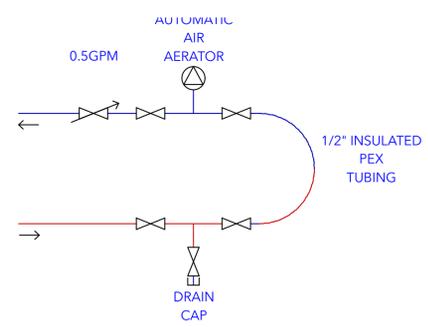
ROOM	AHU 1 TO 8	GPM	FTR 1	GPM	FTR 2	GPM	FTR 3	GPM	CUH 2,3,4	GPM	CUH 15,6,7,8	GPM	UH 1,2,3,4	GPM	TOTAL GPM	
Classroom 133	1	0.50	12	2.16												
Special Ed 132			3	0.54												
Classroom 130	1	0.50	16	2.88												
Classroom 128 Tech	1	0.50	12	2.16												
Classroom 122 Art/Pack	1	0.50	10	2.10												
Reception 12			4	0.72												
Lab 110																
Hallway 127, 126, 129					36	3.61										
Principal 111	1	0.50	4	0.72												
Conference 10A																
Nurse 119																
Early adjacent Kindergarten							4	0.53								
Kindergarten 121	1	0.50	12	2.16					1	0.97						
Classroom 118	1	0.50	16	2.88												
Meeting 135			3	0.54												
Classroom 134	1	0.50	12	2.16												
Boiler and Storage																
Total		4.00		19.63				3.61		0.53				20.07	3.20	53.89

NOTE: Flow Calculation is calculated using a 20F TD @ 200F Supply Temperature 180F Return Temperature

2 TABLE 2 FLOW ADJUSTMENT PER ZONE



3 EXISTING AHU PIPING SCHEMATIC (8) LOCATIONS



4 EXISTING AHU PIPING SCHEMATIC MODIFICATION (8) LOCATIONS

NOT FOR CONSTRUCTION

Drawing Set Type and Issue Date:
Contract Set: 06/16/2016
Rev #: 07/21/2016
As-Built: 08/31/2016

BOILER ROOM SCHEMATIC
CHILMARK SCHOOL
8 State Road Chilmark MA 02535

Date: 1/31/2018
Drawn by: BD
Scale: as noted
Sheet:

M-08

This drawing should not be used for construction unless noted as such.
© 2015 South Mountain Company

Drawing Set Type and Issue Date:
Contract Set: 06/16/2016
Rev #1: 07/21/2016
As-Built: 08/31/2016

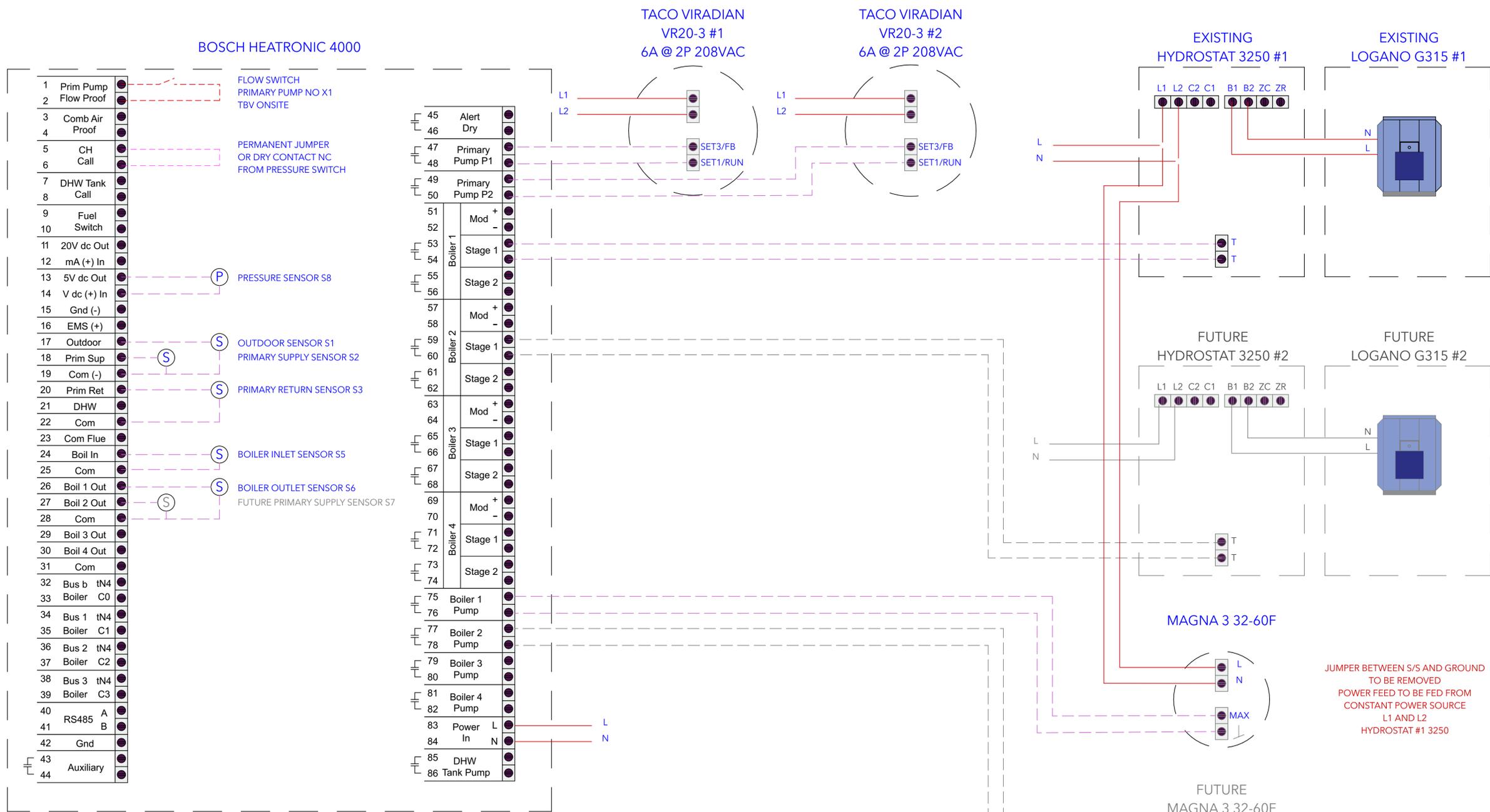
BOILER CONTROL SCHEMATIC

CHILMARK SCHOOL

8 State Road Chilmark MA 02535

Date: 1/31/2018
Drawn by: BD
Scale: as noted
Sheet:

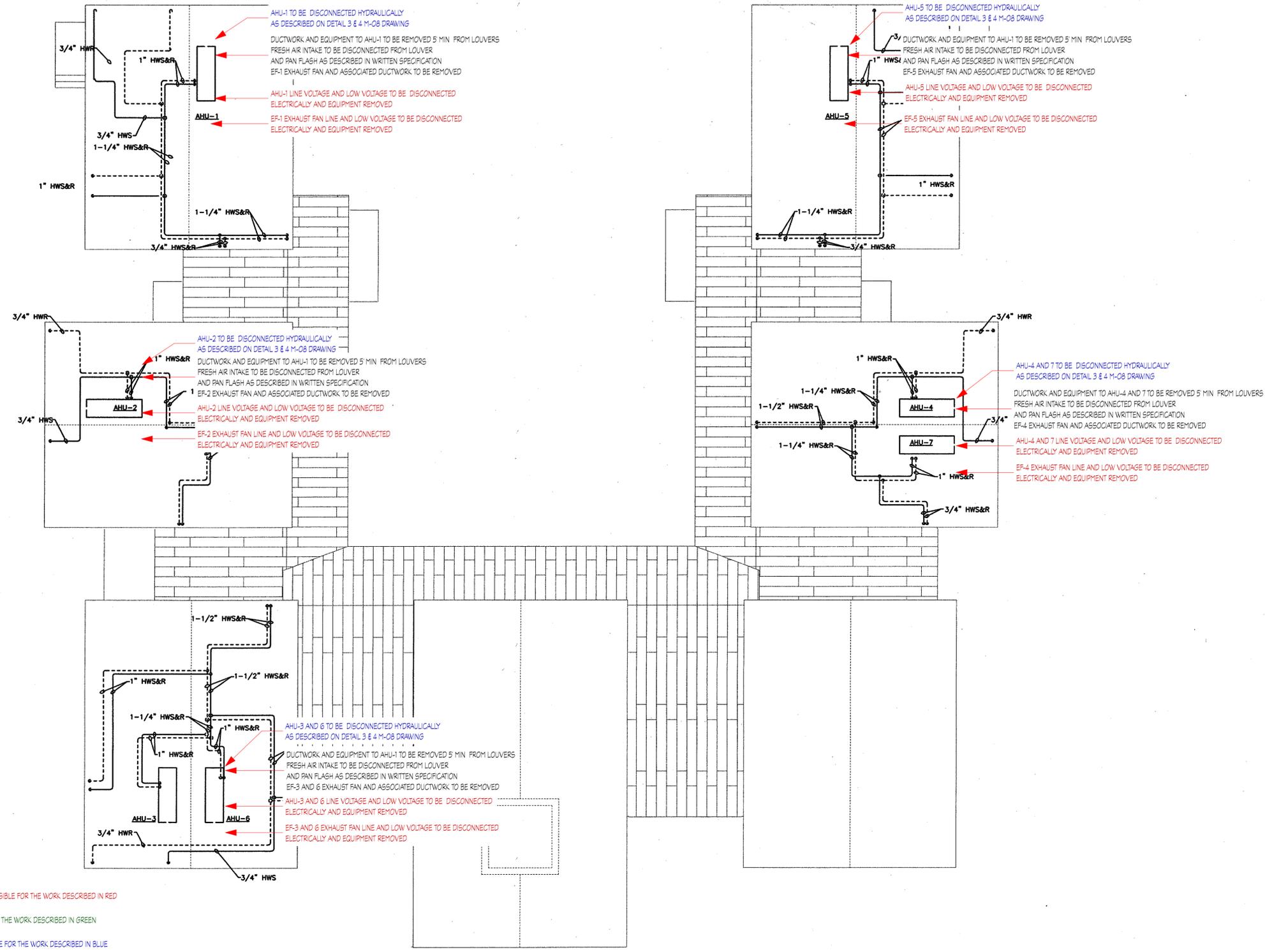
M-09



NOTE: ALL LOW VOLTAGE WIRING TO BE 18/2 AWG
 - - - 18/2 LOW VOLTAGE WIRING
 - - - FUTURE 18/2 LOW VOLTAGE WIRING
 - - - LINE VOLTAGE WIRING
 [] CONTROL ENCLOSURE

JUMPER BETWEEN S/S AND GROUND
TO BE REMOVED
POWER FEED TO BE FED FROM
CONSTANT POWER SOURCE
L1 AND L2
HYDROSTAT #1 3250

NOT FOR CONSTRUCTION



- ← ELECTRICIAN SUBCONTRACTOR IS RESPONSIBLE FOR THE WORK DESCRIBED IN RED
- ← AV SUBCONTRACTOR IS RESPONSIBLE FOR THE WORK DESCRIBED IN GREEN
- ← HEATING SUBCONTRACTOR IS RESPONSIBLE FOR THE WORK DESCRIBED IN BLUE
- ← SMC IS RESPONSIBLE FOR THE WORK DESCRIBED IN BLACK
- ← ALARM SUBCONTRACTOR IS RESPONSIBLE FOR THE WORK DESCRIBED IN PINK

Drawing Set Type and Issue Date:

Contract Set	06/16/2016
Rev #1	07/21/2016
As-Built	08/31/2016

HVAC ATTIC HVAC LAYOUT
CHILMARK SCHOOL
8 State Road Chilmark MA 02535

NOT FOR CONSTRUCTION

THOMPSON AND BOBE ARCHITECTS
 140 CARRIDGE BLVD
 WESTBOROUGH MA 01581
 TEL: 508/865-1100
 FAX: 508/865-1101

ENGINEER: ANTHONY CONNOLLY
 100 STATE ST
 SUITE 100
 WESTBOROUGH MA 01581
 TEL: 508/865-1100
 FAX: 508/865-1101

PROJECT # 2005010
DATE JUN 24, 1998
SCALE NONE
DRAWN BY K.J.P.
CHECKED BY J.M.P.

PROJECT # 2005010
DATE JUN 24, 1998
SCALE NONE
DRAWN BY K.J.P.
CHECKED BY J.M.P.

MENEMSHA SCHOOL
 Chilmark, Martha's Vineyard, Massachusetts

REVISIONS
 NO. DATE
 1 06/24/98
 2 06/24/98
 3 06/24/98

HVAC SCHEDULES

SHEET
H-2
 PROJECT # 2005010

CABINET UNIT HEATER SCHEDULE

UNIT NO.	SERVICE	LOCATION	TYPE	CAPACITY MBH	CFM	MOTOR ELECTRICAL DATA			WATER DATA			MANUFACTURER MODEL (AS STANDARD)	REMARKS
						HP	V/PH/∅Z	W	HP	W	P.S.D. (°F)		
CUH-1	129 HALL-E	129 HALL-E	RECESSED CEILING	40	335	1/10	120/1/∅0	4	200	180	1.5	STERLING RC	(1)
CUH-2	125	CLASSROOM	RECESSED WALL	9.7	75	1/20	120/1/∅0	4	200	180	2.6	BEACON WARRIORS TRIM F.L.O. III	(2)
CUH-3	134	CLASSROOM	RECESSED WALL	9.7	75	1/20	120/1/∅0	4	200	180	2.6	BEACON WARRIORS TRIM F.L.O. III	(2)
CUH-4	131	CLASSROOM	RECESSED WALL	9.7	75	1/20	120/1/∅0	4	200	180	2.6	BEACON WARRIORS TRIM F.L.O. III	(2)
CUH-5	128 HALL-W	128 HALL-W	RECESSED CEILING	40	335	1/10	120/1/∅0	4	200	180	1.5	STERLING RC	(1)
CUH-6	127 HALL-N	127 HALL-N	RECESSED CEILING	40	335	1/10	120/1/∅0	4	200	180	1.5	STERLING RC	(1)
CUH-7	127 HALL-N	127 HALL-N	RECESSED CEILING	40	335	1/10	120/1/∅0	4	200	180	1.5	STERLING RC	(1)
CUH-8	127 HALL-N	127 HALL-N	RECESSED CEILING	40	335	1/10	120/1/∅0	4	200	180	1.5	STERLING RC	(1)

(1) PROVIDE HIGH CAPACITY TWO (2) ROW HEATING COIL.
 (2) FLUSH MOUNTED UNIT.
 (3) FINISH COLOR OF FACE PANELS TO BE SELECTED BY THE ARCHITECT.

UNIT HEATER SCHEDULE

UNIT NO.	LOCATION	TYPE	CAPACITY MBH	CFM	WATTS	ELECTRICAL DATA			WATER DATA			MANUFACTURER MODEL (AS STANDARD)	REMARKS
						V/PH/∅Z	W	HP	W	HP	P.S.D. (°F)		
UH-1	BACKLIFT STORAGE	HORIZONTAL	8	245	9	120/1/∅0	18	200	180	.8	STERLING IS		
UH-2	BACKLIFT STORAGE	HORIZONTAL	8	245	9	120/1/∅0	18	200	180	.8	STERLING IS		
UH-3	BACKLIFT STORAGE	HORIZONTAL	8	245	9	120/1/∅0	18	200	180	.8	STERLING IS		
UH-4	BACKLIFT STORAGE	HORIZONTAL	8	245	9	120/1/∅0	18	200	180	.8	STERLING IS		

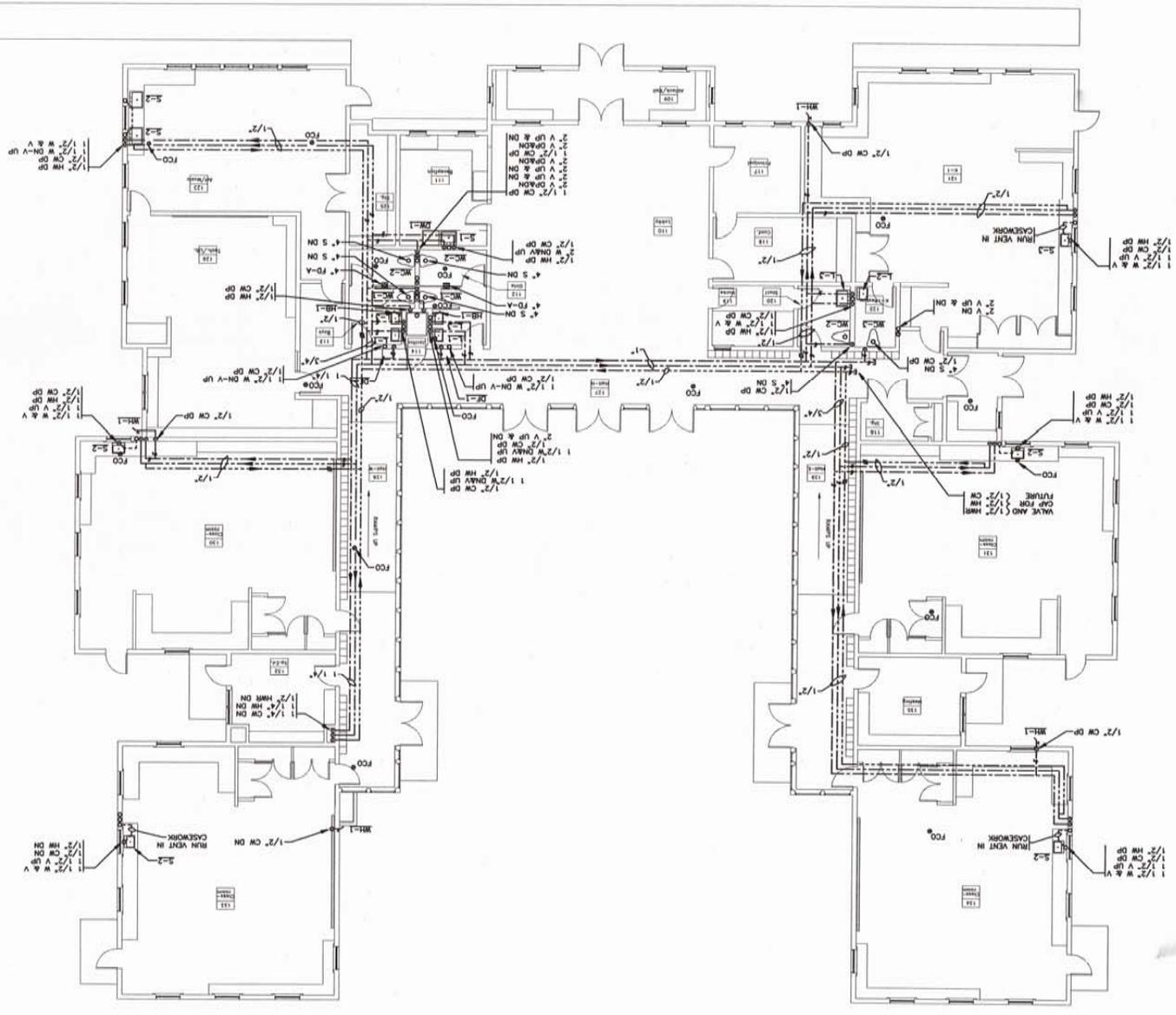
MANUFACTURER MODEL (AS STANDARD)	REMARKS
TRAME	(1) (2) (3)

DIFFUSER, REGISTER & GRILLE SCHEDULE

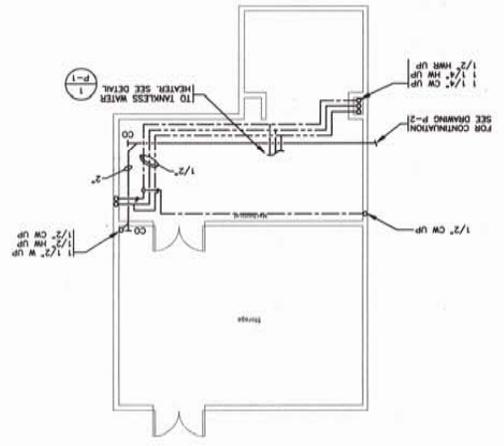
TAG	MONILE SIZE (IN)	SIZE (IN)	NECK SIZE (IN)	MAX CFM	SERVICE	SLOW	MANUFACTURER MODEL (AS STANDARD)			REMARKS
							ITUS - TOCA	ITUS - TOCA	ITUS - TOCA	
CD-1	---	8" x 8"	8"	125	SUPPLY	4-8MM	ITUS - TOCA	ITUS - TOCA	ITUS - TOCA	(1)
CD-2	---	12" x 12"	8"	200	SUPPLY	4-8MM	ITUS - TOCA	ITUS - TOCA	ITUS - TOCA	(1)
CD-3	---	12" x 12"	10"	275	SUPPLY	4-8MM	ITUS - TOCA	ITUS - TOCA	ITUS - TOCA	(1)
CD-4	---	12" x 12"	8"	200	SUPPLY	3-8MM	ITUS - TOCA	ITUS - TOCA	ITUS - TOCA	(1)
CR-1	---	8" x 8"	8" x 8"	125	RETURN	---	ITUS - 3500RL	ITUS - 3500RL	ITUS - 3500RL	(2) (4)
CR-2	---	12" x 12"	12" x 12"	200	RETURN	---	ITUS - 3500RL	ITUS - 3500RL	ITUS - 3500RL	(2) (4)
CR-3	---	12" x 24"	12" x 24"	350	RETURN	---	ITUS - 3500RL	ITUS - 3500RL	ITUS - 3500RL	(2) (4)
CR-4	---	14" x 24"	14" x 24"	650	RETURN	---	ITUS - 3500RL	ITUS - 3500RL	ITUS - 3500RL	(2) (4)
ER-1	---	8" x 8"	8" x 8"	125	EXHAUST	---	ITUS - 3500RL	ITUS - 3500RL	ITUS - 3500RL	(2) (4)
ER-2	---	12" x 12"	12" x 12"	200	EXHAUST	---	ITUS - 3500RL	ITUS - 3500RL	ITUS - 3500RL	(2) (4)
ER-3	---	18" x 8"	18" x 8"	200	EXHAUST	---	ITUS - 3500RL	ITUS - 3500RL	ITUS - 3500RL	(2) (4)
ER-4	---	18" x 10"	18" x 10"	400	EXHAUST	---	ITUS - 3500RL	ITUS - 3500RL	ITUS - 3500RL	(2) (4)
RR-1	---	12" x 8"	12" x 8"	200	RETURN	---	ITUS - 3500RL	ITUS - 3500RL	ITUS - 3500RL	(2) (4)
SR-1	---	12" x 8"	12" x 8"	200	SUPPLY	---	ITUS - 3500RL	ITUS - 3500RL	ITUS - 3500RL	(2) (5)

(1) SURFACE MOUNTED, "HARD CEILING" TYPE
 (2) SURFACE MOUNTED WITH "HARD CEILING" FRAME
 (3) SINGLE DEFLECTION WITH VOLUME DAMPER
 (4) DOUBLE DEFLECTION

FIRST FLOOR PLAN



BASEMENT PART PLAN



THOMAS & MCKEE
 ARCHITECTS
 1400 J
 © 73
 MECHANICAL
 PLUMBING
 ELECTRICAL
 P-1
 SEE DRAWING P-2
 FOR CONTINUATION
 TO INGRESS WATER
 HEATER SEE DETAIL

Chilmark Select Board
Town Hall
401 Middle Road
Chilmark, MA 02535-0119

May 9, 2019

Re: Chilmark School HVAC Project (Phase 2)

In my role as chair of the town's Energy and Finance Advisory Committees, I would like to bring to your attention a number of issues with the above referenced project, which after several years of delay and discussion has still not progressed beyond the preparatory stage. In my opinion, the newly revised UIRSD plans, if carried out, are inappropriate for the school and financially questionable.

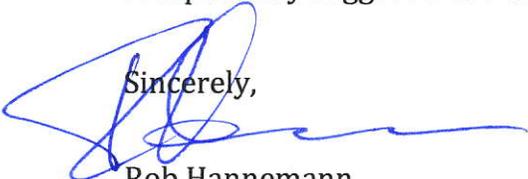
First, the current statement of work is completely different than the work for which we (and the other UIRSD towns) appropriated funds in the spring of 2018. The work contemplated in the new SOW is simply "removal and replacement of selected existing HVAC components". In fact, the plan now is to add an oil-fired boiler and replace one or more water pumps. It does not address the inadequate control systems, the need for insulation in the building to reduce wasted heating energy and increase comfort, or fix the excessively noisy ventilation system installed in an earlier phase. In other words, the plan as I understand it is not responsive to the HVAC issues identified and continually pointed out by the school staff.

Second, the addition of a second oil-fired boiler (as a back up to the relatively new boiler currently providing heat and hot water) is inappropriate for a 21st century municipal building. Installation of an electric heat pump primary HVAC approach, with the existing boiler as backup and hot water supply, will provide both heating and air conditioning – just as the HVAC upgrade to the Community Center will accomplish. Further, over a relatively short period of time I am confident that this approach will provide a significant cost savings for the town and the school district. Green Communities funds are potentially available for a significant fraction of the needed work; not so for the current plan.

Finally, a tour of the building in February revealed that the ventilation system previously installed could be interfering with the sprinkler system in several rooms. I am not a fire safety engineer, but if this is indeed the case we should initiate an inspection by the appropriate fire personnel.

I respectfully suggest that a Select Board review of this project is in order.

Sincerely,



Rob Hannemann

Cc: Susan Stevens, Head of School
Robert Lionette

Chilmark School HVAC Project Outline

When complete, the school will have an up-to-date HVAC system based on heat pump electric heat, with the existing oil-fired circulating water system as backup for heating (and the domestic hot water source). Controls will be distributed for the classroom and office spaces. Ventilation will be energy efficient, using energy recovery systems. Heat pumps will supply air conditioning for spring and fall hot weather.

Project outline:

1. Insulate all attic spaces at the roofline, to at least code level.
2. Complete the upgrade of existing oil-fired boiler system (variable speed circulating pumps, appropriate controls compatible with addition of heat pumps, potential extension of some baseboard units).
3. Removal of defunct boiler and obsolete air handlers
4. Design and equipment selection for heat pump system.
5. Installation of heat pumps external units, air handlers, and refrigerant coils.
6. Move ERVs to attic space as originally envisioned (addresses noise problem).
7. Upgrade control system.
8. Ensure integrity of fire suppression system.
9. Procure and install backup generator.

Heat Pump v. Oil Heating Operational Costs

As a starting point, assume 1 gallon of oil:

- 2019 price ~ \$2.78
- Energy content ~ 137,381 BTU
- Delivered heat at 85% efficiency of oil/hydronic system ~ 116,744 BTU

Now examine a cold climate heat pump:

- Modern coefficient of performance (Northeast US climate conditions) over an entire heating season ~ 3.2
- That means to deliver the amount of heat equivalent to a gallon of oil is $116,744/3.2 = 36,482$ BTU of electrical energy
- Converting that to kWh: $36,482/3412 = 10.7$ kWh
- 2019 all-in Eversource electricity price estimate ~ \$0.25 per kWh
- Therefore, the cost to provide this heat is ~ \$2.68

Thus, the heat pump operational cost is about 4% less than oil heat.

Note also that oil prices will likely increase while electricity prices will decrease over the life of the project.

6. List **ONLY** Those Prime And Sub-Consultant Personnel Specifically Requested In The Advertisement. This Information Should Be Presented Below In The Form Of An Organizational Chart. Include Name Of Firm And Name Of The One Person In Charge Of The Discipline, With Mass. Registration Number, As Well As MBE/WBE Status, If Applicable:

CHILMARK SCHOOL
Town of Chilmark & Up Island
Regional School District

Prime Consultant
Principal-In-Charge

Project Manager for Study

Project Manager for Design

Discipline
(from advertisement)

Name Of Firm
Person In Charge Of Discipline
Mass. Registr. #
MBE/WBE Certified (If
Applicable)

Discipline
(from advertisement)

Name Of Firm
Person In Charge Of Discipline
Mass. Registr. #
MBE/WBE Certified (If
Applicable)

Discipline
(from advertisement)

Name Of Firm
Person In Charge Of Discipline
Mass. Registr. #
MBE/WBE Certified (If
Applicable)

Discipline
(from advertisement)

Name Of Firm
Person In Charge Of Discipline
Mass. Registr. #
MBE/WBE Certified (If
Applicable)

7. Brief Resume of ONLY those Prime Applicant and Sub-Consultant personnel requested in the Advertisement. <u>Include Resumes of Project Managers</u> . Resumes should be consistent with the persons listed on the Organizational Chart in Question # 6. Additional sheets should be provided only as required for the number of Key Personnel requested in the Advertisement and they must be in the format provided. By including a Firm as a Sub-Consultant, the Prime Applicant certifies that the listed Firm has agreed to work on this Project, should the team be selected.	
a. Name and Title Within Firm:	a. Name and Title Within Firm:
b. Project Assignment:	b. Project Assignment:
c. Name and Address Of Office In Which Individual Identified In 7a Resides: <div style="text-align: right;"> MBE <input type="checkbox"/> WBE <input type="checkbox"/> SDVOBE <input type="checkbox"/> VBE <input type="checkbox"/> </div>	c. Name and Address Of Office In Which Individual Identified In 7a Resides: <div style="text-align: right;"> MBE <input type="checkbox"/> WBE <input type="checkbox"/> SDVOBE <input type="checkbox"/> VBE <input type="checkbox"/> </div>
d. Years Experience: With This Firm: _____ With Other Firms: _____	d. Years Experience: With This Firm: _____ With Other Firms: _____
e. Education: Degree(s) /Year/Specialization	e. Education: Degree(s) /Year/Specialization
f. Active Registration: Year First Registered/Discipline/Mass Registration Number	f. Active Registration: Year First Registered/Discipline/Mass Registration Number
g. Current Work Assignments and Availability For This Project:	g. Current Work Assignments and Availability For This Project:
h. Other Experience and Qualifications Relevant To The Proposed Project: (Identify Firm By Which Employed, If Not Current Firm):	h. Other Experience and Qualifications Relevant To The Proposed Project: (Identify Firm By Which Employed, If Not Current Firm):

8a. Current and Relevant Work By Prime Applicant Or Joint-Venture Members. Include ONLY Work Which Best Illustrates Current Qualifications In The Areas Listed In The Advertisement (List Up To But Not More Than 5 Projects).					
a. Project Name And Location Principal-In-Charge	b. Brief Description Of Project And Services (Include Reference To Relevant Experience)	c. Client's Name, Address And Phone Number (Include Name Of Contact Person)	d. Completion Date (Actual Or Estimated)	e. Project Cost (In Thousands)	
				Construction Costs (Actual, Or Estimated If Not Completed)	Fee for Work for Which Firm Was Responsible
(1)					
(2)					
(3)					
(4)					
(5)					

8b. List Current and Relevant Work By Sub-Consultants Which Best Illustrates Current Qualifications In The Areas Listed In The Advertisement (Up To But Not More Than 5 Projects For Each Sub-Consultant). Use Additional Sheets Only As Required For The Number Of Sub-Consultants Requested In The Advertisement.

Sub-Consultant Name:

a. Project Name and Location Principal-In-Charge	b. Brief Description Of Project and Services (Include Reference To Relevant Experience	c. Client's Name, Address And Phone Number. Include Name Of Contact Person	d. Completion Date (Actual Or Estimated)	e. Project Cost (In Thousands)	
				Construction Costs (Actual, Or Estimated If Not Completed)	Fee For Work For Which Firm Was/Is Responsible
(1)					
(2)					
(3)					
(4)					
(5)					

9. List All Projects Within The Past 5 Years For Which Prime Applicant Has Performed, Or Has Entered Into A Contract To Perform, Any Design Services For All Public Agencies Within The Commonwealth.

# of Total Projects:		# of Active Projects:	Total Construction Cost (In Thousands) of Active Projects (excluding studies):		
Role P, C, JV *	Phases St., Sch., D.D., C.D.,A.C.*	Project Name, Location and Principal-In-Charge	Awarding Authority (Include Contact Name and Phone Number)	Construction Costs (In Thousands) (Actual, Or Estimated If Not	Completion Date (Actual or Estimated) (R)Renovation or (N)New
		1.			
		2.			
		3.			
		4.			
		5.			
		6.			
		7.			
		8.			
		9.			
		10.			
		11.			
		12.			

* P = Principal; C = Consultant; JV = Joint Venture; St. = Study; Sch. = Schematic; D.D. = Design Development; C.D. = Construction Documents; A.C. = Administration of Contract

10. Use This Space To Provide Any Additional Information Or Description Of Resources Supporting The Qualifications Of Your Firm And That Of Your Sub-Consultants For The Proposed Project. If Needed, Up To Three, Double-Sided 8 ½" X 11" Supplementary Sheets Will Be Accepted. **APPLICANTS ARE ENCOURAGED TO RESPOND SPECIFICALLY IN THIS SECTION TO THE AREAS OF EXPERIENCE REQUESTED IN THE ADVERTISEMENT.**

Be Specific – No Boiler Plate

11. Professional Liability Insurance:

Name of Company	Aggregate Amount	Policy Number	Expiration Date
-----------------	------------------	---------------	-----------------

12. Have monies been paid by you, or on your behalf, as a result of Professional Liability Claims (in any jurisdiction) occurring within the last 5 years and in excess of \$50,000 per incident? Answer **YES** or **NO**. If YES, please include the name(s) of the Project(s) and Client(s), and an explanation (attach separate sheet if necessary).

13. Name Of Sole Proprietor Or Names Of All Firm Partners and Officers:

Name	Title	MA Reg #	Status/Discipline	Name	Title	MA Reg #	Status/Discipline
a.				d.			
b.				e.			
c.				f.			

14. If Corporation, Provide Names Of All Members Of The Board Of Directors:

Name	Title	MA Reg #	Status/Discipline	Name	Title	MA Reg #	Status/Discipline
a.				d.			
b.				e.			
c.				f.			

15. Names Of All Owners (Stocks Or Other Ownership):

Name And Title	% Ownership	MA. Reg.#	Status/Discipline	Name And Title	% Ownership	MA. Reg.#	Status/Discipline
a.				d.			
b.				e.			
c.				f.			

16. I hereby certify that the undersigned is an Authorized Signatory of Firm and is a Principal or Officer of Firm. I further certify that this firm is a "Designer", as that term is defined in Chapter 7C, Section 44 of the General Laws, or that the services required are limited to construction management or the preparation of master plans, studies, surveys, soil tests, cost estimates or programs. The information contained in this application is true, accurate and sworn to by the undersigned under the pains and penalties of perjury.

Submitted by _____ Printed Name and Title _____ Date _____
 (Signature)